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CONCEPT STORMWATER MANAGEMENT PLAN

for

BRISBANE WATER LEGACY VILLAGE REDEVELOPMENT

at

51-57 MASONS PARADE POINT FREDERICK

J	Job No: NL201088						
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D	ate:	1	5.09.21				
			BY	DATE			
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	Checked		DH	15.09.21			
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1. INTRODUCTION

Northrop Consulting Engineers has been engaged by Grindley Pty Ltd to undertake conceptual civil and stormwater design and documentation for the development of the proposed Brisbane Water Legacy Village Residential Apartments at 51-57 Masons Parade, Point Frederick. This report accompanies, and should be read in conjunction with, drawings NL201088 C1.1 – C6.1.

The purpose of this report is to summarise the proposed design solutions for the stormwater management for the Development Application submission to Central Coast Council. The proposed design has been considered with regard to Central Coast Council DCP (Gosford 2013), Central Coast Council Civil Works Specification as well as industry best practice.

We note the information contained in this report is not intended to present detailed design solutions but rather provide solutions commensurate with a conceptual design suitable for Development Application assessment.

2. SITE DESCRIPTION

The subject site is bounded by a multi-storey residential developments to the north, east and south; and Masons Parade to the west.

The site is currently consists of an existing low rise aged care facility with an existing open channel running through the northern boundary of the site.

Figure 1 presents an aerial overview of the site.



Figure 1: Aerial Image of Site (obtained from https://maps.six.nsw.gov.au/)



3. PROPOSED DEVELOPMENT

The proposed development consists of a demolition of a number of existing dwellings, and construction of a new multi-story aged care residential development with on-grade carpark, circulation road and additional undercroft carparking. Additional office and communal areas are located on the ground floor of the development. Landscaping, communal and activity areas are provided at the rear of the development.

The proposed development footprint occupies the northern portion of the site, with the remain site area to be retained and unaffected.

Access to the site will be achieved via Masons Parade. The layout for the development can be seen within drawings NL201088 C1.1 - C6.1.

4. PROPOSED STORMWATER MANAGEMENT STRATEGY

4.1 GENERAL STRATEGY

The onsite stormwater management system has been designed to replicate the processes which would naturally occur onsite. The proposed development will incorporate a number of devices and measures aimed at providing adequate and responsible management of stormwater runoff for minor and major storm events.

In line with Chapter 6.7 of Central Coast Council DCP 2013, the conceptual stormwater management strategy has considered the following items which will be discussed in the following sections of this report:

- Stormwater capture and disposal;
- Water conservation;
- Stormwater retention;
- Stormwater quality;
- Onsite detention;
- Local overland drainage;
- Flooding.

4.2 STORMWATER CAPTURE AND DISPOSAL

Concept stormwater management plans have been prepared for the proposed development and are appended to the rear of this report. The majority of the development area is of a suspended structure built form. The methods of stormwater capture and disposal are outlined below and are to be designed in accordance with AS3500.3 as well as Central Coast Council Engineering Guidelines.

- Runoff from the roof of the residential tower will be captured via a conventional roof drainage system. Once the roof runoff is captured, it will then be conveyed to the rainwater harvesting tank.
- The rainwater harvesting will have a high-level overflow to the stormwater system.
- Runoff from the balcony and podium areas will also be captured by conventional drainage systems and conveyed to the stormwater system on the eastern side of the development, bypassing the rainwater tank.
- Runoff from the carpark and circulation road will be captured and conveyed to the stormwater system, discharging into the northern open channel via water quality treatment devices. Small run-off that cannot be drained back to this location will be captured and conveyed to the kerb & gutter along the Masons Parade road frontage.



• A stormwater system will be installed on the southern side of the development site divert any drainage lines that will be impacted by the new development towards the existing stormwater connection to Masons Parade in the west.

4.2 WATER CONSERVATION

The water conservation objective for the proposed development is to reduce potable water demand by 40% using the provisions nominated within the BASIX report. In summary, it is proposed that the redevelopment will incorporate the following water saving measures:

- Using water efficient fixtures for shower heads, toilet cisterns, toilet taps and kitchen taps including undertaking regular maintenance of these fixtures;
- The use of water efficient dishwashers;
- Landscaping with plant species that require minimal watering and irrigation with appropriate systems to minimise water loss and evaporation. This includes native plant species, using mulch around garden beds, avoiding watering when it's windy, watering during the coolest parts of the day and using drip irrigation;
- Harvested rainwater from part of the roof is proposed to be collected and reused for hardstand washdown, carwash bay and irrigation of landscaping areas.

It is our opinion that the measures outlined above will provide adequate reduction in potable demand to meet the intent of the water conservation target. For detailed assessment of the proposed water conservation initiatives proposed for the development, refer to the project specific BASIX report.

4.2 RETENTION

The intent of water retention targets in Chapter 6.7 of DCP 2013 is to mimic the natural catchment hydrology from all development sites, in terms of:

- Quantity the annual volume of stormwater reaching natural creeks and waterways;
- Rate the peak flow rates leaving the site; and
- Response the time it takes for rain to runoff the site.

To satisfy the intent of the retention targets in the DCP it is proposed to incorporate stormwater source controls to the impervious catchments for the site. In order for stormwater source controls to be effective, they need to have sufficient capacity to meet the above targets. Sizing of controls is described in The Hunter & Central Coast Water Smart Model Planning document (HCCREMS, 2012). Sizing is based on the concept of mitigation of increased stormwater runoff arising from impervious surfaces, for rainfall events with an average recurrence interval of 3 months.

The depth of stormwater runoff that must be captured by the stormwater source controls in order to achieve frequent discharge mitigation is termed the mitigation depth. The mitigation depth for various soil types and are shown below in Table 1.



Soil Texture	Mitigation Depth (mm)
Sand	14
Sandy Loam	14
Clay Loam	10
Clay	7

	Table 1	ŝ	Mitigation	Dep	oth
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Based on geotechnical investigations performed on site, a clay soil profile is considered to best represent the soils to be encountered on site.

The volume of stormwater runoff that must be captured by a source control to achieve frequent discharge mitigation relative to the impervious surfaces that drain to the control is referred to as the mitigation storage and is calculated as shown below:

 $MS = (MIC \times MD) / 1000$

where: MS

MIC = managed impervious catchment (m^2)

= mitigation storage (m^3)

MD = mitigation depth (mm)

Using this method, the following mitigation storage for the impervious areas of the proposed development is calculated as shown below:

Mitigation depth	= 7mm	(clay soil type)
Mitigation area	= 3 720 m ²	(62% impervious)
Mitigation Storage	= [(3 720) x 7] / 1 000)
	= 26 m ³	

Using this method, the total mitigation storage, or retention storage required is 26 m³. It is proposed that a roof area of 1450 m² will drain to the below ground reuse tank with a total of 42kL storage capacity. The additional storage capacity provided will ensure that there is suitable reuse volume provided to meet the demand of the project. The reuse is proposed to be used for irrigation and hardstand washdown.

To ensure that there is adequate draw down, a MUSIC model was used to assess the efficiency of the reuse tank.

The assumed water usage rates are outlined as follows;

Irrigation usage = 1 L/m2/day(NSW modelling guidelines)

The reuse tank demand and efficiency are outlined below.

Table 2 – Reuse Tank Demands								
Reuse Tank	Tank size	Irrigation Area						
Tank 1	42 kL	2.28 kL/Day	79.13%	2 280 m ²				

As can be seen from Table 2, adequate draw down can be achieved based on the proposed tank sizing and reuse scheme.



4.2 STORMWATER QUALITY

In order to minimise adverse impacts upon the ecology of downstream watercourses, stormwater treatment devices have been incorporated into the design of the development. The adopted nutrient and pollution targets were taken from the Central Coast Council Engineering Guidelines and are summarised in Table 3:

Table 3 – Required Water Nutrie Pollutant Criteria	Required Reduction Target (%)
Total Suspended Solids (TSS)	80
Total Phosphorous (TP)	45
Total Nitrogen (TN)	45
Gross Pollutants	90

The performance of the proposed stormwater management strategy was assessed against these targets using the conceptual design software MUSIC (Version 6). The MUSIC model was developed using parameters recommended in the document "NSW MUSIC Modelling Guidelines" (WBM, 2015) and the Central Coast Council (Lowland - Wyong) MUSIC Link.

The total catchment area was divided into separate sub-catchments representing the areas draining to the different treatment devices. A schematic of the MUSIC model is provided in Figure 2.

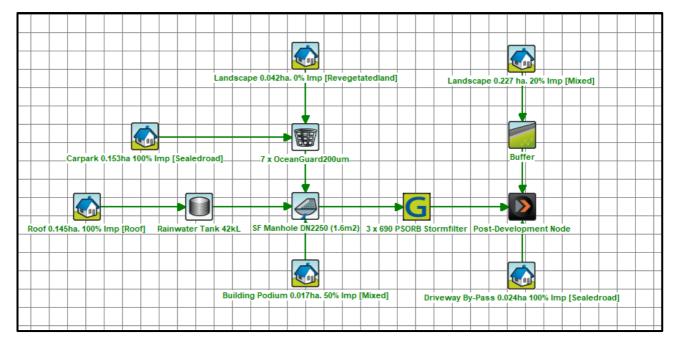


Figure 2 – MUSIC Model Schematic

A number of factors were identified in order to select the most appropriate stormwater quality improvement devices (SQIDs). The proposed development footprint and usage was considered especially significant to this design which eliminated a number of effective treatment options. In addition to the practical constraints, maintenance, operability and aesthetics were considered.

The proposed treatment train incorporates:

 Rainwater Harvesting Tank – Runoff from roof areas is to be directed to a below-ground rainwater harvesting tank. The tank is to be fitted with a proprietary first-flush device which will effectively remove dead insects, bird and animal droppings and concentrated tannic acids from the stormwater system. The rainwater tank will also provide secondary treatment by acting as an initial sediment trap, collecting suspended solids and nutrients attached to those sediments. The volume collected in the harvesting tank is to be reused as described previously in this report. SPEL Stormsack – Pit filter inserts are proposed to provide primary treatment for the ground floor on grade carparking area. The filter inserts will prevent ingress of gross pollutants into the stormwater system.

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- **Pit Filter Inserts** Propriety filter insterts (Psorb filter cartridges or similar) actively filter stormwater runoff, removing suspendered nutrients such as nitrogen and phosphorus, as well as fine suspended solids and small amounts of hydrocarbons.
- Grass buffer runoff from the landscaped spaces will flow over grass buffer strips prior to entering the stormwater system which will allow infiltration and reduce nutrient runoff from the site.

Source node have been adopted from the NSW MUSIC Modelling Guideline (BMT WBM, 2015). Proprietary treatment nodes have been adopted from SPEL and Ocean Protect. The MUSIC modelling results for the above-mentioned treatment strategy are shown below in Table 4:

Pollutant Criteria	Reduction Target (%)	Sources (kg/yr)	Residual Load (kg/yr)	Achieved Reduction (%)
Total Suspended Solids (TSS)	80	951	184	80.7
Total Phosphorous (TP)	45	1.82	0.672	63.2
Total Nitrogen (TN)	45	11.4	5.2	54.5
Gross Pollutants	90	120	10.7	91.1

Table 4 – MUSIC Modelling Results

Note: The MUSIC model can be provided to Council upon request.

Table 4 shows that the proposed stormwater quality management strategy will achieve the required load reduction targets. A copy of the MUSIC Link report has been appended to the rear of this report.

4.5 ONSITE DETENTION

The site is located immediately upstream of the local catchment outlet to Brisbane Water. Providing onsite detention for sites in the lower third of a catchment can have detrimental impacts to the peak discharge from the catchment as providing detention has the potential to delay the peak flow leaving the site and coinciding with the larger peak of the upstream catchment.

As such, onsite detention is not required for this development and has as not been included.

4.6 LOCAL OVERLAND DRAINAGE

An overland flow path has been provided within the site to convey excess stormwater runoff towards the northern open channel via the internal circulation road.

4.7 FLOODING

The site is impacted by two separate flood events, the first being the overland surface flow generated from the upstream catchment and the second being foreshore flooding from the Brisbane Water foreshore.

Both flood events have been detailed in flood studies previously commissioned by Central Coast Council prepared by Cardno. The flood information certificate obtained from Central Coast Council can be found in Appendix A.

Flood behaviour

Overland Surface Flow

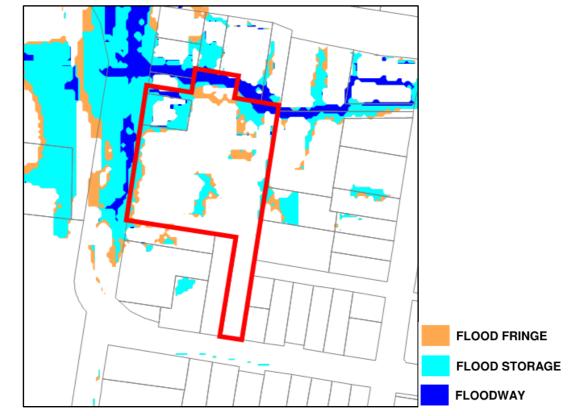
Figure 3 presents the 1% AEP peak flood depths for the site as extracted from the Flood Information Certificate provided by Central Coast Council. It is noted that the flood behaviour observed is reflective of the Gosford CBD Local Overland Flow Flood Study prepared by Cardno (2013).



Figure 3 – 1% AEP Peak Flood Depths (Flood Information Certificate - CCC)

It is observed that the site is impacted by overland surface flow flooding, with the majority of the flood extents contained within the existing channel along the northern boundary, and a small extent of flooding observed along the street frontage of Masons Parade to the west. Additional pockets of ponding are identified in the centre of the site. However, these are attributed to localised trapped low points created by the obstruction of existing buildings.

Figure 4 presents the hydraulic category for the flood extents.

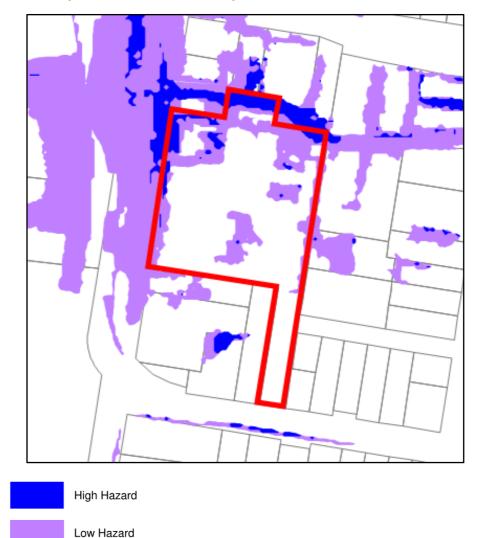






A combination of Flood Fringe and Flood Storage are observed scattered on the site with the clearly defined stormwater channel classified as Floodway in the north.

The flood hazard categories are illustrated in Figure 5.





The site is primarily only impacted by low hazard flood extents, with the exception of the channelised flow to the north.



The PMF peak flood depths are presented in Figure 6.

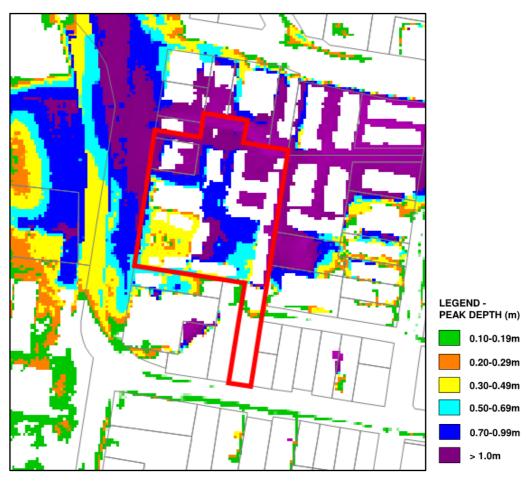


Figure 6 – PMF Peak Flood Depths (Cardno 2013 – Excerpt of Figure 4.5)

It is observed that the site is impacted by the PMF event when assessing the overland flow. The peak depths observed are a result of the impedance and restriction of flow modelled for the existing dwellings on site.

Brisbane Water Foreshore Flooding

The second major flood event that affect the subject site has been detailed in the 'Brisbane Water Foreshore Flood Study' prepared by Cardno (2013). The report details the impacts of flooding as a result of the Brisbane Water Foreshore, including storm bursts, wave effects and sea level rise.

Figure 7 presents an excerpt of the flood extents determined as part of the study.

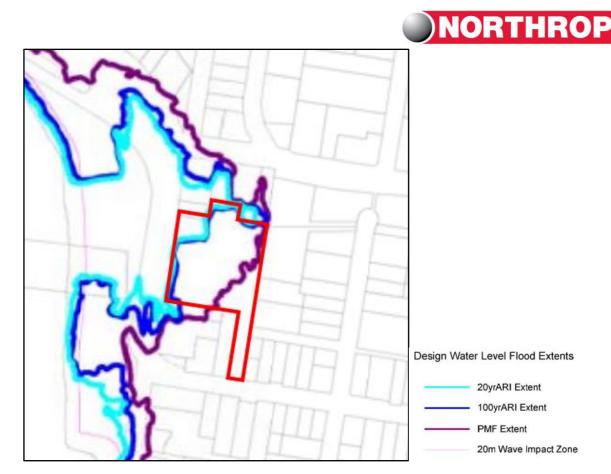


Figure 7 – Design Water Level Flood Extents (Cardno 2013 – Excerpt of Figure 6.16A)

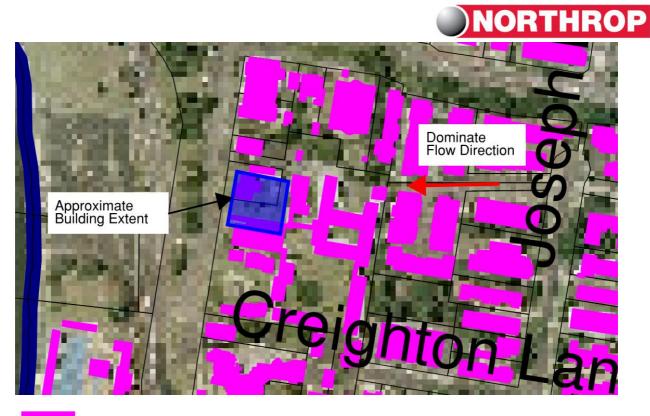
It is observed that the site is only affected on the fringes of the site boundary in both the 5% and 1% AEP storm events. The PMF storm event is seen to inundate the majority of the site.

The flood levels were extracted from the flood study in the location of the subject site.

- 1% AEP = 1.71m AHD
- 1% AEP + 500mm freeboard = 2.21m AHD
- 1% AEP + 0.55m MSLR = 2.26m AHD
- PMF = 2.46m AHD

Flood Impacts - 1% AEP and PMF Flood Events

Figure 8 presents the building extents that was utilised for the Cardno overland flow study with the approximate proposed building extents overlayed. The existing building on the subject site are proposed to be demolished.



Building Outline

Figure 8 – Flood Model Obstructions (Cardno 2013 – Excerpt of Figure 3.5)

It can be observed that the proposed building extent is consistent or less than that currently adopted within the flood study. It can be reasonably determined, that when considering the flood impacts of the proposed development for the 1% AEP and PMF flood events, that the proposed development will not adversely affect the existing flood behaviour for the neighbouring properties. The proposed development may reduce the severity of flooding for surrounding properties as a number of existing buildings will be demolished and removed from the site, reducing the amount of blockage for any flows traversing through the site.

It is also noted that the effective cross-section for the open channel has not been reduced at any location through the site, and the proposed maintenance & garbage building is located outside of the existing 1% AEP flood extents.

Floor Levels

It is proposed that the floor levels of all habitable and non-habitable spaces are to be at or above the PMF level consistent with the controls for 'Seniors Housing'.

The floor level has been proposed to satisfy the highest flood level for the range of events including:

- Overland Flow:
 - 1% AEP + 500mm Freeboard = 2.36m AHD; or
 - PMF Event = 2.78m AHD

Or

- Foreshore Flooding:
 - \circ 1% AEP Flood Level + Sea Level Rise (50-year Design life) = 2.26m AHD; or
 - \circ 1% AEP Flood Level + 500mm Freeboard = 2.21m AHD; or
 - \circ PMF Flood Level = 2.46m AHD.

Note: Flood levels were obtained from the worst case levels within the footprint of the proposed development.



Access Roads, Driveways and Parking Areas

The requirements for all access roads, driveways and external parking areas to be above the 1% AEP flood level is deemed ineffective for this development, as it is noted that the main street access in Masons Parade is inundated during the 1% AEP flood event preventing the ability to safely receive and evacuate occupants without crossing floodwaters. As such, the inclusion of this requirement in the design is deemed redundant, as it does not achieve the intended outcome.

On-site refuge can be sought on-site during extreme flooding events, as the floor level of habitable and non-habitable spaces will be above the PMF level. Given the relatively short duration of the PMF flooding event, it is proposed that this is deemed acceptable, given the location of the site and surround flood hazards. Emergency access can be achieved towards the Central Coast Highway south of the site.

Earthworks & Site Filling

The site is identified to only contain small areas of flooding extent identified as flood storage, with the remaining areas classified as flood fringe, with the exception of the open channel north of the site.

It is proposed that the filling within the identified flooding extents shall be offset by providing the equivalent storage capacity elsewhere on-site, to ensure no significant adverse impacts on the flood behaviour for neighbouring and adjacent properties.

An 3D earthworks model was developed to compare the volume of storage lost by the proposed development, to the 1% flood level of 1.86m. It was calculated that 380m³ of potential flood storage would be lost due to the earthworks required to facilitate the development.

It is proposed that the existing open channel is locally widened to provide the 380m3 of offset flood storage required to mitigate any potential impacts.

The extent of filling required for the site when considering the potential flood impacts of the foreshore flooding event is deemed to have an inconsequential impact on the flood behaviour, given the relative volumes of fill compared to the volumes observed within the water body. Any filling will likely have an immeasurable and neglectable impact on surrounding flood levels.

Flood Summary

The flood characteristics of the site have been discussed, outlining the two major flood events that affect the proposed development. A review of Council's flood studies has been performed including discussion on the existing and proposed site impacts.

It has been demonstrated how the proposed development addresses the requirements of the Gosford DCP 2013, in particular Chapter 6.7 – Water Cycle Management (6.7.7.6 Flooding Targets). Discussion has been provided outlining the justification to not utilise an extensive 2D hydraulic flood model to demonstrate the flooding objectives can be achieved and instead provide qualitative assessment of the proposed development in conjunction with the previously prepared Flood Studies commissioned by Central Coast Council.



5. CONCLUSION

The proposed stormwater management design presented above has been prepared to comply with Central Coast Council (Gosford) DCP and Central Coast Council Design Guidelines as well as best industry practice. The design philosophy is based on the principle of at source treatment, to reduce conveyance infrastructure and manage water quantity and quality aspects.

Based on the above, our conceptual investigation and concept designs indicate the proposed development can adequately manage and address all items surrounding stormwater runoff. Should you have any queries, please feel free to contact the undersigned on (02) 4365 1668.

R. Such

Robert Suckling

Hallie

Daniel Holland

Civil Engineer

Civil Engineer



REFERENCES:

Gosford Development Control Plan 2013

Central Coast Council, Civil Works Specification – Design Guideline 2018

BMT WBM Pty Ltd, New South Wales MUSIC Modelling Guidelines, August 2015

Central Coast Council, Water Sensitive Urban Design – Technical Guideline No 3. – Device Selection Guide, November 2010.

Gosford CBD Overland Flow Flood Study – Cardno 2013

Brisbane Water Foreshore Flood Study - Cardno 2013



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APPENDIX A – SUPPLEMENTARY INFORMATION

- Concept Stormwater Management Plan -
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- MUSIC Link Report Flood Information Certificate -

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Job No: Job Name: Pages: NL201088 BRISBANE WATER LEGACY VILLAGE 1 of 1 From Robert Suckling Description Date BRISBANE WATER LEGACY VILLAGE RESIDENTIAL Day 21 10 15 APARTMENTS 51-57 MASONS PDE. POINT FREDERICK Month 05 09 09 INTERNAL CIVIL WORKS 21 21 21 Year Doc No. **Document Title** Revision C1.1 COVER SHEET В А В CONCEPT SEDIMENT & EROSION CONTROL C2.1 В А А В PLAN C2.2 SEDIMENT & EROSION CONTROL DETAILS В Α В STORMWATER MANAGEMENT & LEVELS C4.1 В В A А PLAN LONG SECTIONS & CROSS SECTIONS -C5.1 в Revision В A SHEET 1 C6.1 Α VEHICLE SWEPT PATHS В В Current

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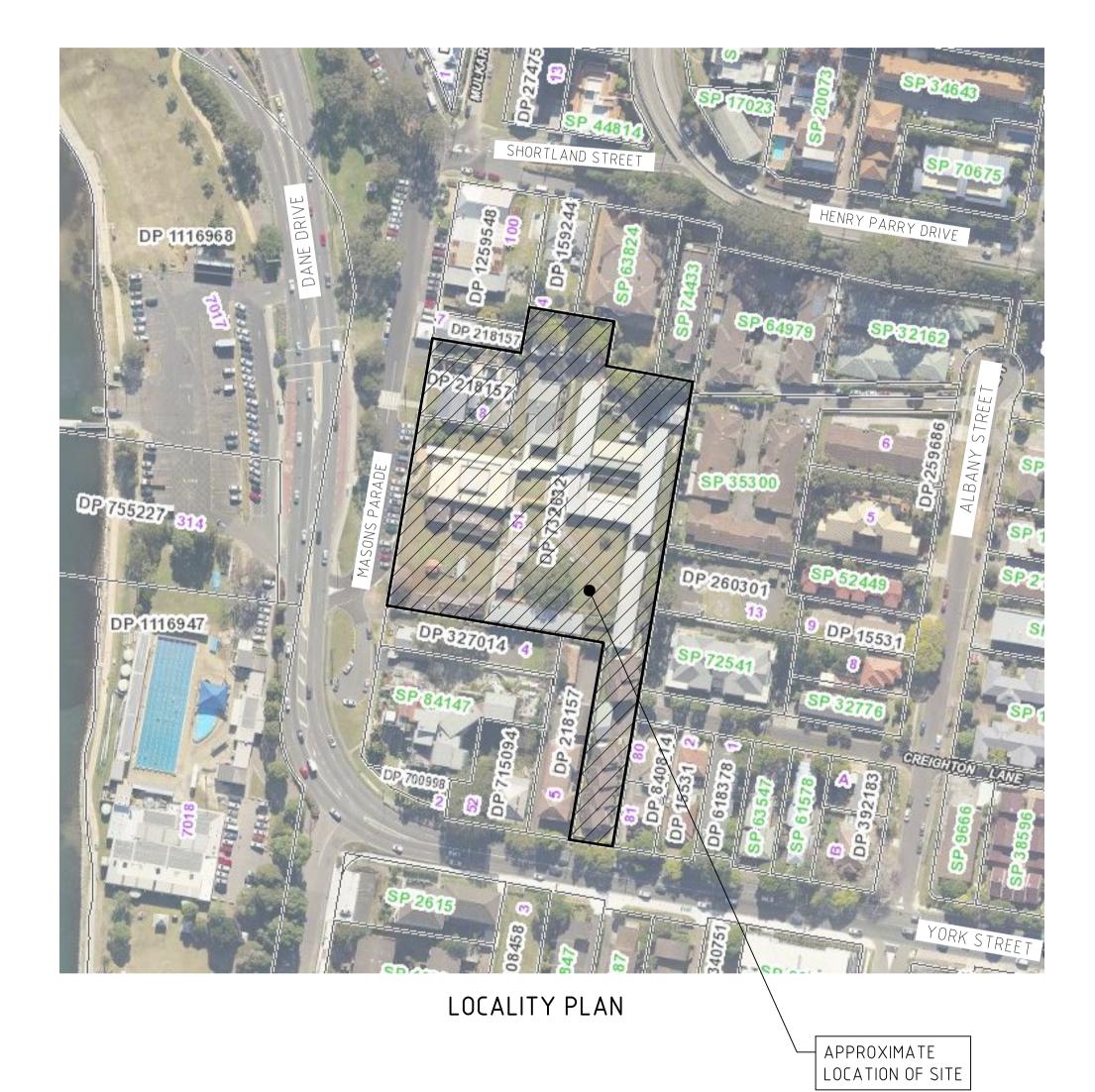
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BRISBANE WATER LEGACY VILLAGE RESIDENTIAL APARTMENTS

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C2.2	SEDIMENT & EROSION CONTROL DETAILS
C4.1	STORMWATER MANAGEMENT & LEVELS PLAN
C5.1	LONG SECTIONS & CROSS SECTIONS – SHEET 1
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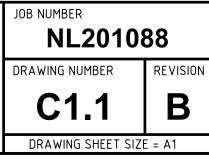
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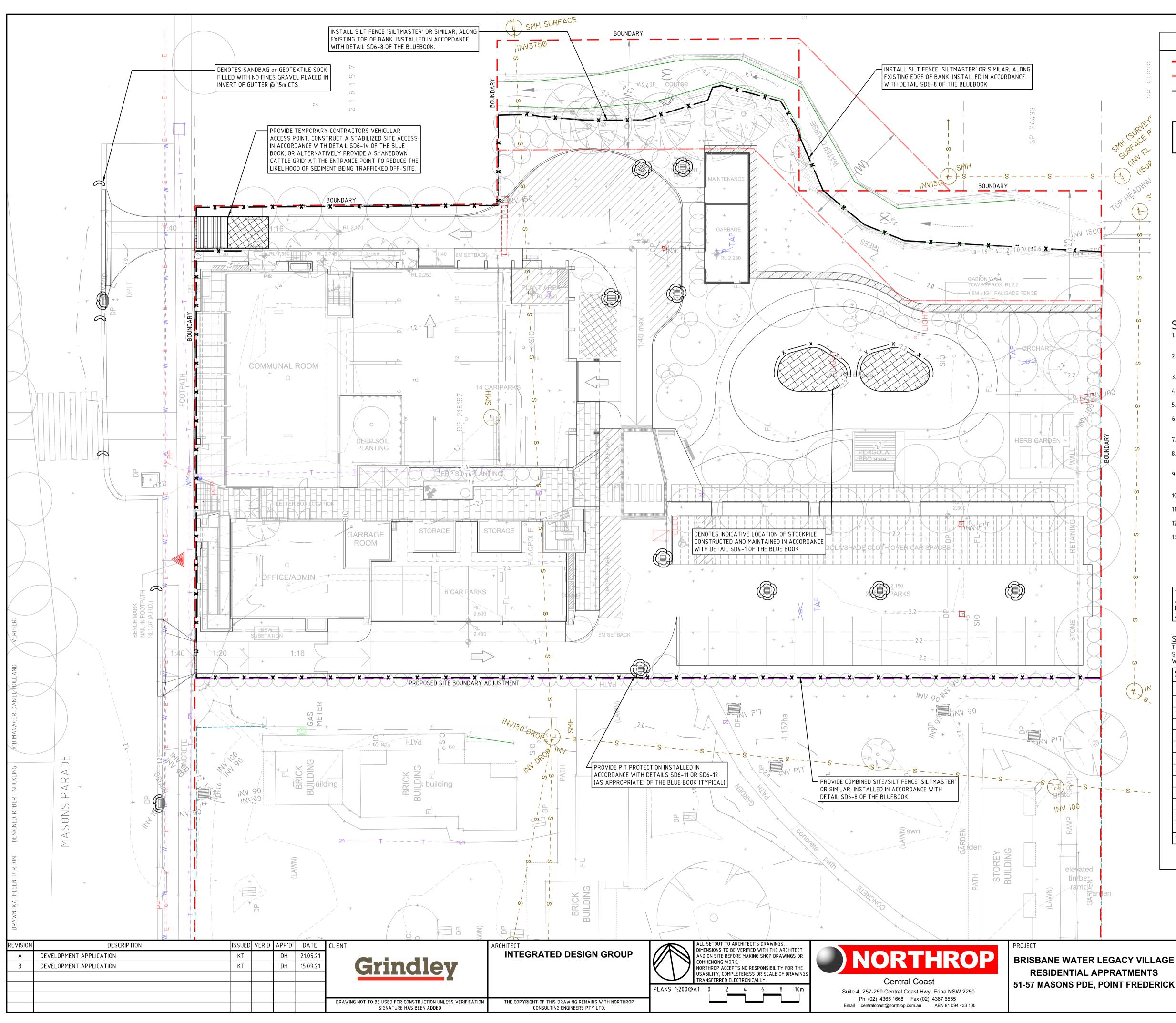


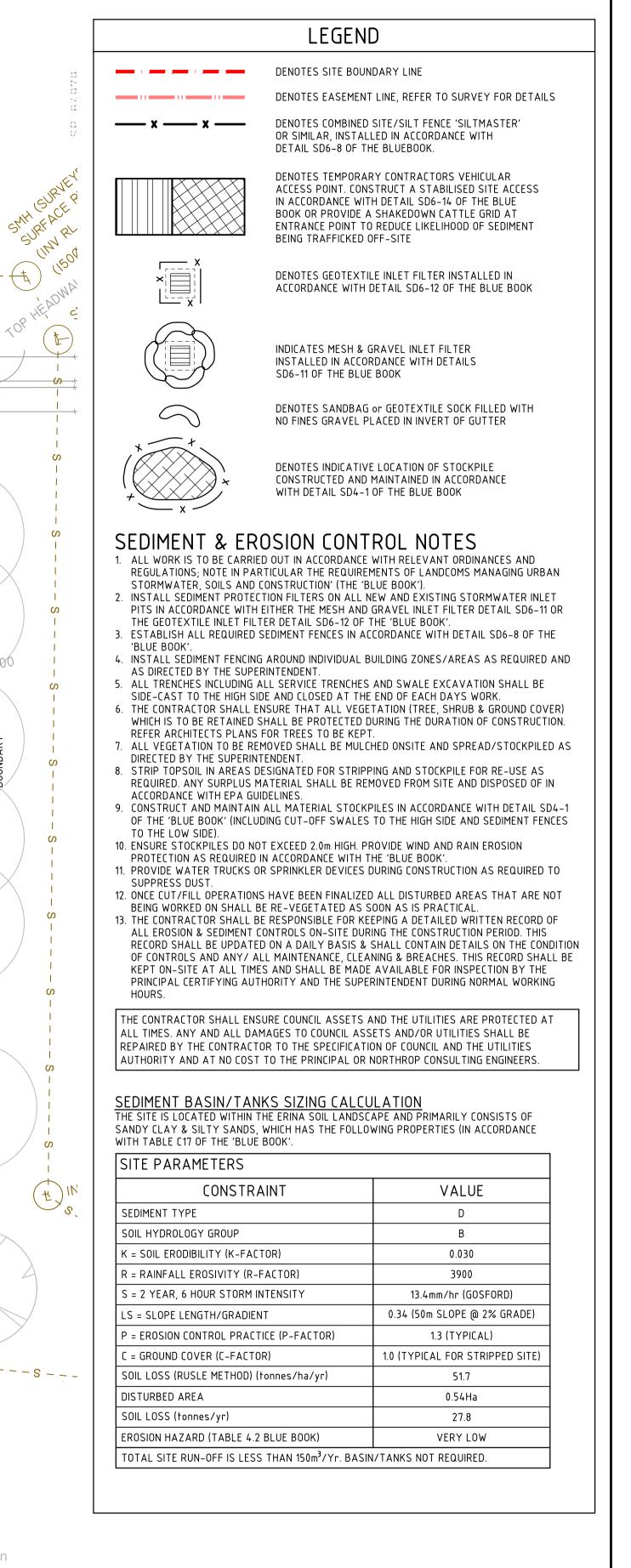
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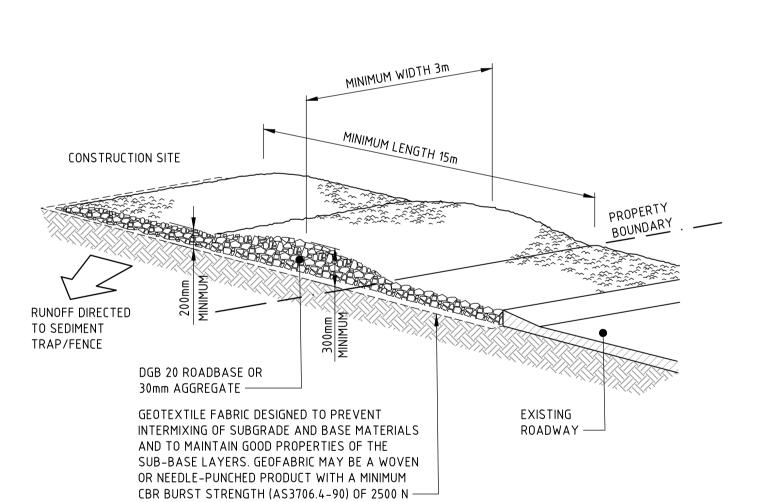
- 1. STRIP THE TOPSOIL, LEVEL THE SITE AND COMPACT THE SUBGRADE.

- 2. COVER THE AREA WITH NEEDLE-PUNCHED GEOTEXTILE.

- 3. CONSTRUCT A 200mm THICK PAD OVER THE GEOTEXTILE USING ROAD BASE OR 30mm AGGREGATE.

- 4. ENSURE THE STRUCTURE IS AT LEAST 15 METRES LONG OR TO BUILDING ALIGNMENT AND AT LEAST 3 METRES WIDE.
- 5. WHERE A SEDIMENT FENCE JOINS ONTO THE STABILISED ACCESS, CONSTRUCT A HUMP IN THE STABILISED ACCESS TO DIVERT WATER TO THE SEDIMENT FENCE.

STABILISED SITE ACCESS (SD 6-14)



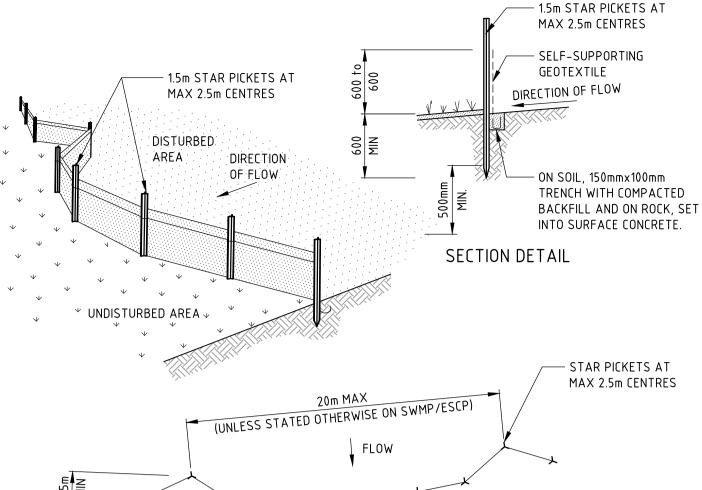
SEDIMENT FENCE (SD 6-8)

OF THE TRENCH. ENSURE ANY STAR PICKETS ARE FITTED WITH SAFETY CAPS. 4. FIX SELF-SUPPORTING GEOTEXTILE TO THE UPSLOPE SIDE OF THE POSTS ENSURING IT GOES TO THE BASE OF THE TRENCH. FIX THE GEOTEXTILE WITH WIRE TIES OR AS RECOMMENDED BY THE MANUFACTURER. ONLY USE GEOTEXTILE SPECIFICALLY PRODUCED FOR SEDIMENT FENCING. THE USE OF SHADE CLOTH FOR THIS PURPOSE IS

6. BACKFILL THE TRENCH OVER THE BASE OF THE FABRIC AND COMPACT IT THOROUGHLY OVER THE GEOTEXTILE.

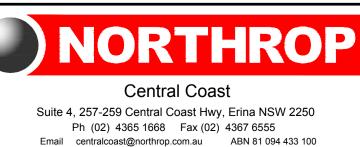
5. JOIN SECTIONS OF FABRIC AT A SUPPORT POST WITH A 150mm OVERLAP.

- ENTRENCHED. DRIVE 1.5 METRE LONG STAR PICKETS INTO GROUND AT 2.5 METRE INTERVALS (MAX) AT THE DOWNSLOPE EDGE 3.
- 50 LITRES PER SECOND IN THE DESIGN STORM EVENT, USUALLY THE 10-YEAR EVENT. 2. CUT A 150mm DEEP TRENCH ALONG THE UPSLOPE LINE OF THE FENCE FOR THE BOTTOM OF THE FABRIC TO BE
- CONSTRUCT SEDIMENT FENCES AS CLOSE AS POSSIBLE TO BEING PARALLEL TO THE CONTOURS OF THE SITE, BUT WITH SMALL RETURNS AS SHOWN IN THE DRAWING TO LIMIT THE CATCHMENT AREA OF ANY ONE SECTION. THE CATCHMENT AREA SHOULD BE SMALL ENOUGH TO LIMIT WATER FLOW IF CONCENTRATED AT ONE POINT TO
- FLOW PLAN CONSTRUCTION NOTES



-	тыс			WITH	NORTHROP	
	1 113	DRAWING	REMAINS	WIIII	NUKTHKUP	
sι	JLTIN	G ENGINEE	RS PTY L	TD.		

LL SETOUT TO ARCHITECT'S DRAWINGS, DIMENSIONS TO BE VERIFIED WITH THE ARCHITECT AND ON SITE BEFORE MAKING SHOP DRAWINGS OR COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED ELECTRONICALLY.



PROJECT **BRISBANE WATER LEGACY VILLAGE RESIDENTIAL APPRATMENTS** 51-57 MASONS PDE, POINT FREDERICK

5. CONSTRUCT EARTH BANKS (STANDARD DRAWING 5-5) ON THE UPSLOPE SIDE TO DIVERT WATER AROUND

4. WHERE THEY ARE TO BE IN PLACE FOR MORE THAN 10 DAYS, STABILISE FOLLOWING THE APPROVED ESCP OR SWMP TO REDUCE THE C-FACTOR TO LESS THAN 0.10.

STOCKPILES (SD 4-1)

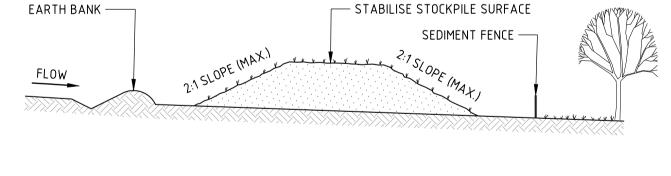
3. WHERE THERE IS SUFFICIENT AREA, TOPSOIL STOCKPILES SHALL BE LESS THAN 2m IN HEIGHT.

STOCKPILES AND SEDIMENT FENCES (STANDARD DRAWING 6-8) 1 TO 2m DOWNSLOPE.

- 2. CONSTRUCT ON THE CONTOUR AS LOW, FLAT, ELONGATED MOUNDS.
- FLOW, ROADS AND HAZARD AREAS.

- 1. PLACE STOCKPILES MORE THAN 2m (PREFERABLY 5m) FROM EXISTING VEGETATION, CONCENTRATED WATER

- CONSTRUCTION NOTES





- KERB-SIDE INLET

GRAVEL-FILLED WIRE MESH

OR GEOTEXTILE 'SAUSAGE'

– OVERFLOW

GRAVEL-FILLED WIRE MESH

2. FABRICATE A SLEEVE MADE FROM GEOTEXTILE OR WIRE MESH LONGER THAN THE LENGTH OF THE INLET PIT

4. PLACE THE FILTER AT THE OPENING LEAVING AT LEAST A 100mm SPACE BETWEEN IT AND THE KERB INLET.

6. SANDBAGS FILLED WITH GRAVEL CAN SUBSTITUTE FOR THE MESH OR GEOTEXTILE PROVIDING THEY ARE

PLACED SO THAT THEY FIRMLY ABUT EACH OTHER AND SEDIMENT-LADEN WATERS CANNOT PASS BETWEEN.

NOTE: THIS PRACTICE ONLY TO BE USED WHERE

SPECIFIED IN APPROVED SWMP/ESCP.

3. FORM AN ELLIPTICAL CROSS-SECTION ABOUT 150mm HIGH x 400mm WIDE.

5. FORM A SEAL WITH THE KERB TO PREVENT SEDIMENT BYPASSING THE FILTER.

OR GEOTEXTILE 'SAUSAGE'

TIMBER SPACER TO SUIT

 \checkmark

FILTERED WATER

TIMBER SPACER TO SUIT.

RUNOFF WATER WITH

CONSTRUCTION NOTES

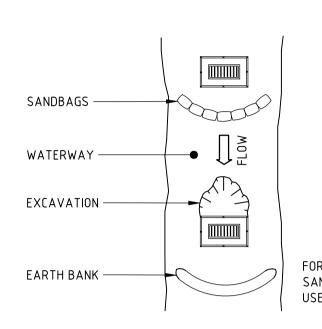
SEDIMENT —

1. INSTALL FILTERS TO KERB INLETS ONLY AT SAG POINTS.

AND FILL IT WITH 25mm TO 50mm GRAVEL.

MAINTAIN THE OPENING WITH SPACER BLOCKS.

SEDIMENT.



1 METRE MAX.

STAR PICKETS —

CONSTRUCTION NOTES

- 1. FABRICATE A SEDIMENT BARRIER MADE FROM GEOTEXTILE OR STRAW BALES.

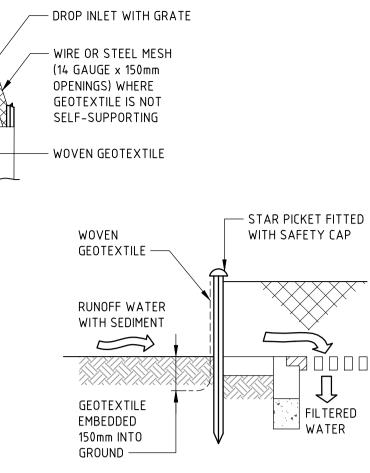
- STRAW BALES OR GEOFABRIC. REDUCE THE PICKET SPACING TO 1 METRE CENTRES.

- 3. IN WATERWAYS, ARTIFICIAL SAG POINTS CAN BE CREATED WITH SANDBAGS OR EARTH BANKS AS SHOWN IN
- THE DRAWING.

- TO BYPASS IT.







FOR DROP INLETS AT NON-SAG POINTS, SANDBAGS, EARTH BANK OR EXCAVATION USED TO CREATE ARTIFICIAL SAG POINT

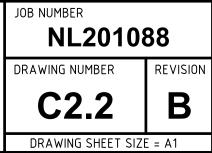
2. FOLLOW STANDARD DRAWING 6-7 AND STANDARD DRAWING 6-8 FOR INSTALLATION PROCEDURES FOR THE

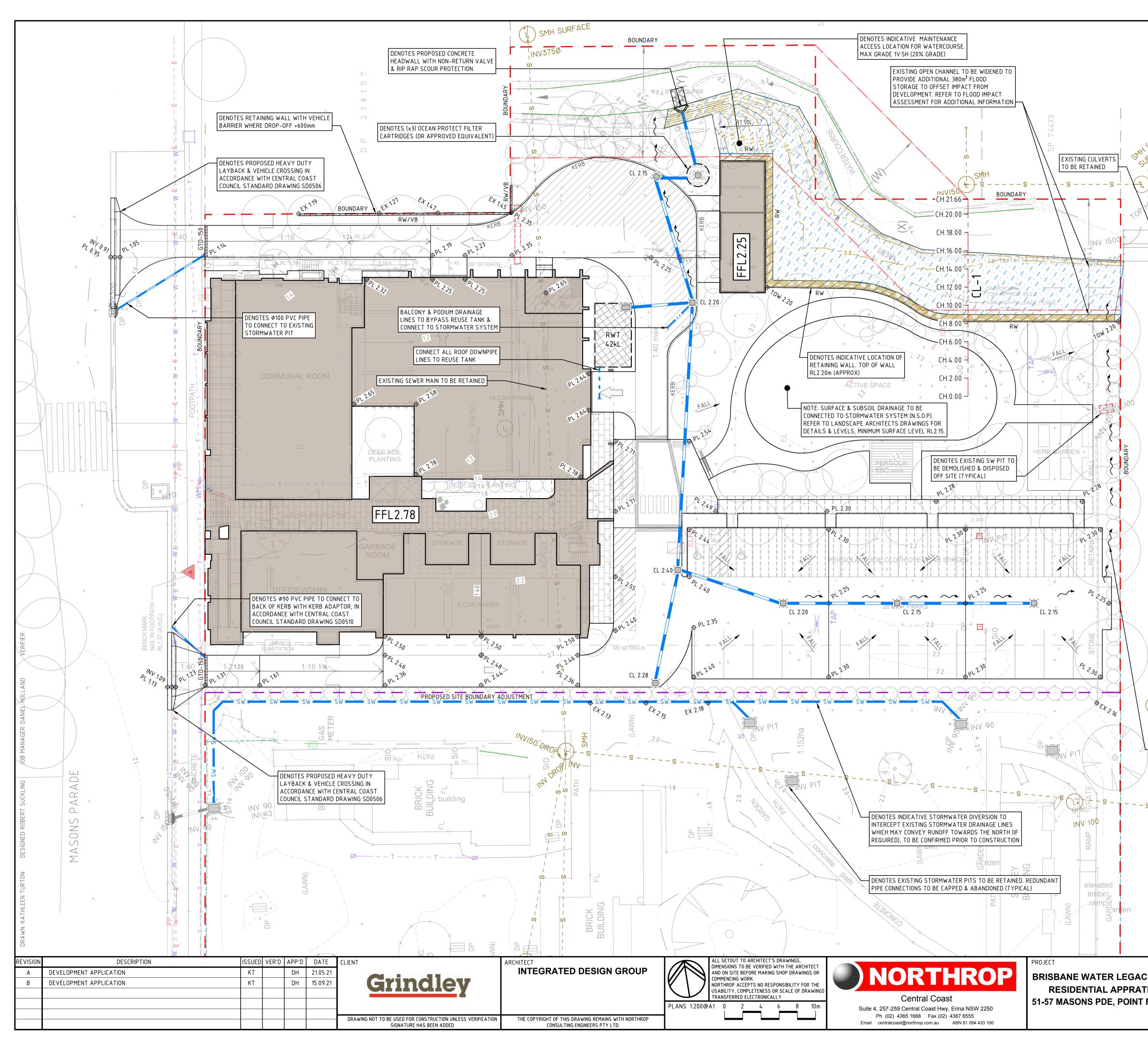
4. DO NOT COVER THE INLET WITH GEOTEXTILE UNLESS THE DESIGN IS ADEQUATE TO ALLOW FOR ALL WATERS

GEOTEXTILE INLET FILTER (SD 6–12)

NOT FOR CONSTRUCTION DRAWING TITLE

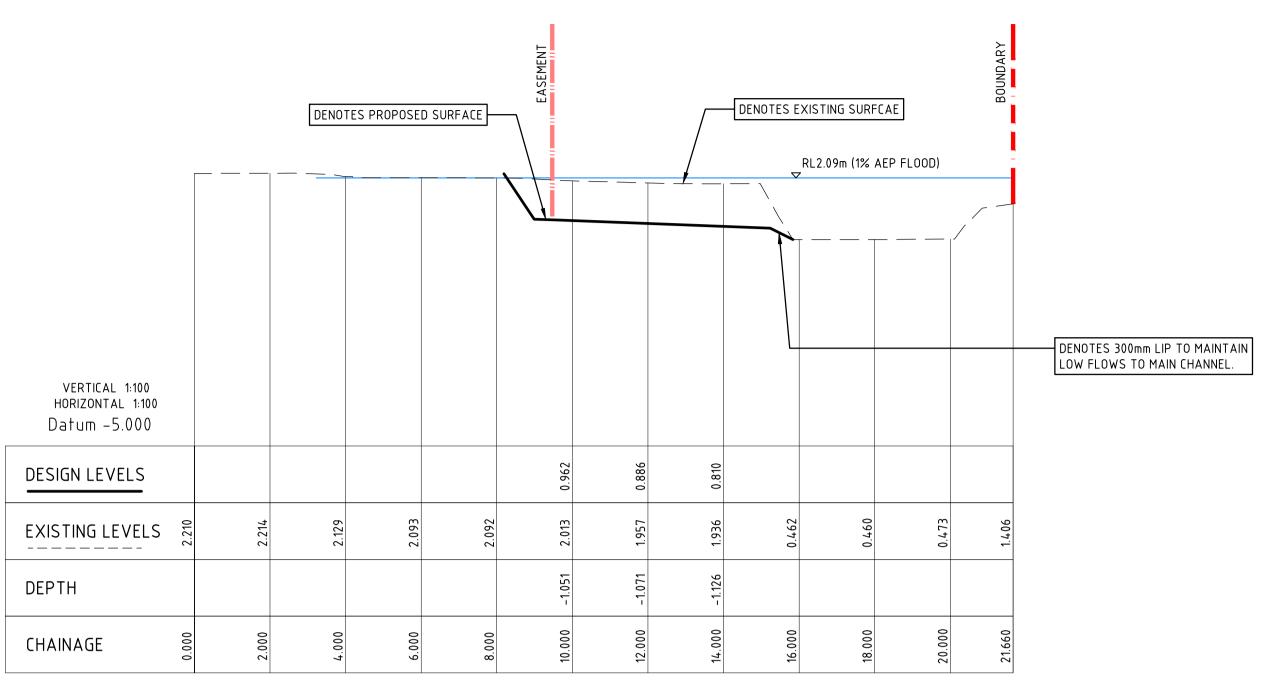
INTERNAL CIVIL WORKS **SEDIMENT & EROSION** CONTROL DETAILS





		LEGEND		
0.70		DENOTES SITE BOUNDARY LINE		
		DENOTES EASEMENT LINE, REFER DENOTES PROPOSED BUILDING EX	TENTS, REFER TO	
		ARCHITECTURAL & STRUCTURAL		
SURVEY BRACE P UNN RL	FFL2.78	DENOTES PROPOSED FINISHED FLO	JOR LEVEL	
REAL	Φ ^{PL 2,3V}	DENOTES PROPOSED FINISHED SU		
	PL 2.30 ← CL 2.15 ← EX 2.15	DENOTES PROPOSED STORMWATE		
HEADWA	Φ ^ε ^Γ	DENOTES EXISTING CONTOURS		
	-1.0	DENOTES DESIGN CONTOURS		
CH0.00				
	CL-1	DENOTES ALIGNMENT CONTROL LI REFER TO LONG SECTION	NE & CHAINAGE,	
		DENOTES PROPOSED STORMWATE INLET PITS ARE TO BE FITTED WIT ACCORDANCE WITH MANUFACTUR DENOTES EXISTING STORMWATER BE RETAINED	TH FILTER INSERTS IN ERS SPECIFICATION	
	GTD-150	DENOTES GRATED TRENCH DRAIN	& WIDTH	
 		DENOTES CONCRETE HEADWALL V AND RIP RAP SCOUR PROTECTION		:
S	RWT	DENOTES BELOW GROUND RAINW/ COMBINED CAPACITY. HARVESTEE FOR IRRIGATION & TOILET FLUSHI	RAINWATER TO BE USED	
	\mathbf{v}	DENOTES PROPOSED STORMWATE DENOTES OVERLAND FLOW PATH	R LINE	
	RW/VB	DENOTES RETAINING WALL WITH (REQUIRED FOR DROP-OFFS GREA		
۱ ۵ —	——————————————————————————————————————	DENOTES APPROXIMATE LOCATIO ELECTRICITY LINE	N OF EXISTING	
	— — — G — — ——	DENOTES APPROXIMATE LOCATIO		
		DENOTES APPROXIMATE LOCATIO TELECOMMUNICATION LINE DENOTES APPROXIMATE LOCATIO		
	— — — S — — —			
BU	UILDER IS RESPONSIBLE FOR L	ES ARE APPROXIMATE ONLY & MA DCATING EXISTING INFRASTRUCTUI (ELS ETC) PRIOR TO COMMENCING C	RE (CULVERTS, PITS, PIPE	
	HE BUILDER SHALL ALLOW TO	MODIFY ALL EXISTING SERVICE CO ITH THE RELEVANT AUTHORITIES F	VERS TO MATCH THE NEW	
	ROVIDE TEMPORARY TRAFFIC	CONTROL IN ACCORDANCE WITH ST	ATE & FEDERAL STATUT	ORY
		IAN HEIGHT DATUM (AHD). ORIGIN		\exists
	RAWINGS TO BE READ IN	CONJUNCTION WITH CONCEPT LOOD IMPACT ASSESSMENT	STORMWATER	
·	DENOTES INDICATIVE OVERLAN	ID FLOW		
	PATH TO BE FREE OF OBSTRU	TIONS		
S				
		ORIGINAL DRAWING IS IN COLOUR	www.1100	0.com.au
	DRAWING TITLE	FOR CON	STRUCT	ION
	INTERNAL		NL2010	
MENTS FREDERICK		R MANAGEMENT ELS PLAN	DRAWING NUMBER	REVISION

DRAWING SHEET SIZE = A1



CL-1 FLOOD OFFSET STORAGE SECTION

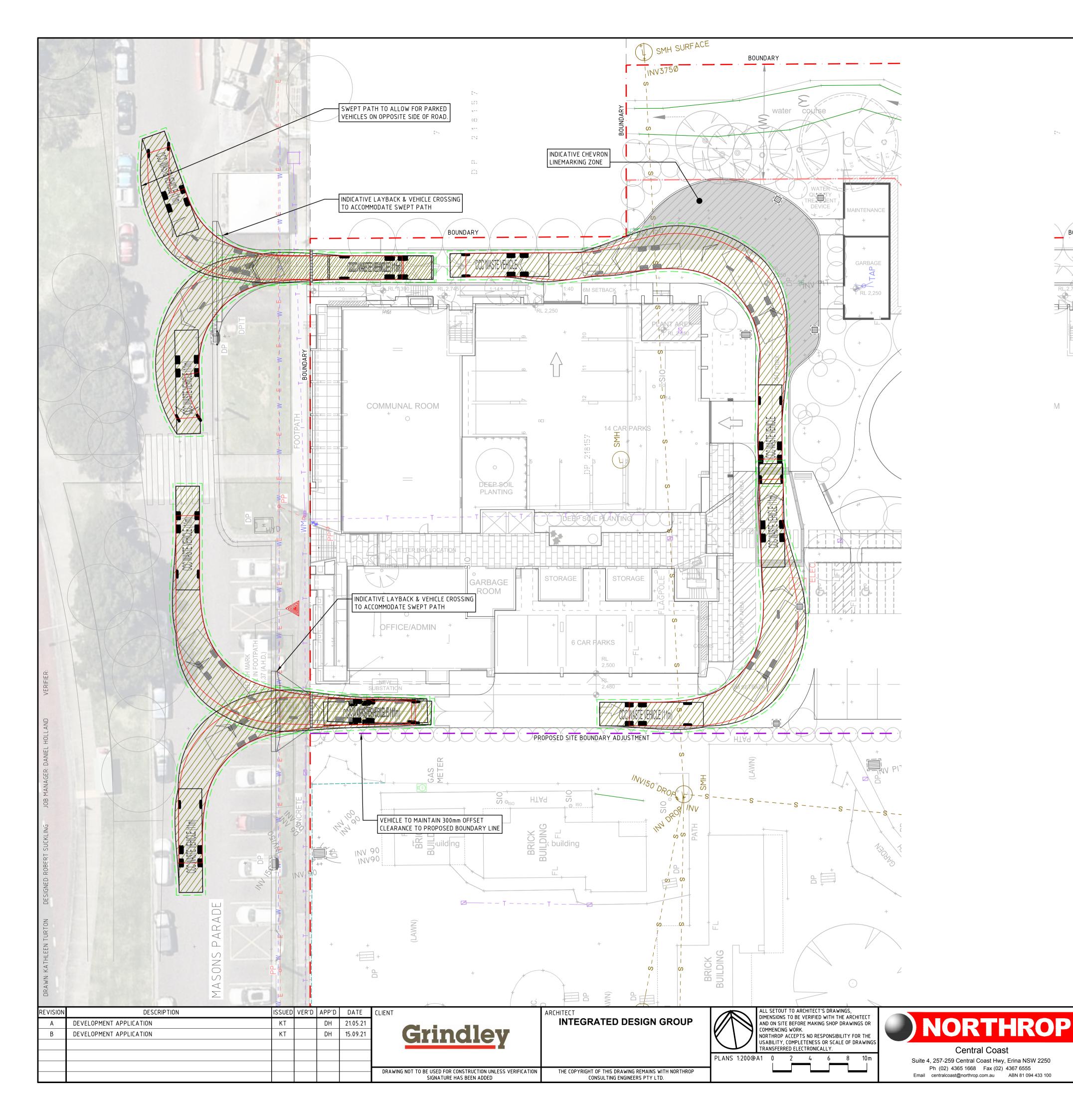
REVISION A B	DESCRIPTION DEVELOPMENT APPLICATION DEVELOPMENT APPLICATION	ISSUED VER'D APP'D DATH KT DH 21.05. KT DH 15.09.		ARCHITECT INTEGRATED DESIGN GROUP	ALL SETOUT TO ARCHITECT'S DRAWINGS, DIMENSIONS TO BE VERIFIED WITH THE ARCHITECT AND ON SITE BEFORE MAKING SHOP DRAWINGS OR COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED ELECTRONICALLY.	Central Coast	PROJECT BRISBANE WATER LE RESIDENTIAL APP 51-57 MASONS PDE, PC
			DRAWING NOT TO BE USED FOR CONSTRUCTION UNLESS VERIFICATION SIGNATURE HAS BEEN ADDED	THE COPYRIGHT OF THIS DRAWING REMAINS WITH NORTHROP CONSULTING ENGINEERS PTY LTD.	VERT 1:100@A1 0 1 2 3 4 5m HORIZ 1:100@A1 0 1 2 3 4 5m	Suite 4, 257-259 Central Coast Hwy, Erina NSW 2250 Ph (02) 4365 1668 Fax (02) 4367 6555 Email centralcoast@northrop.com.au ABN 81 094 433 100	

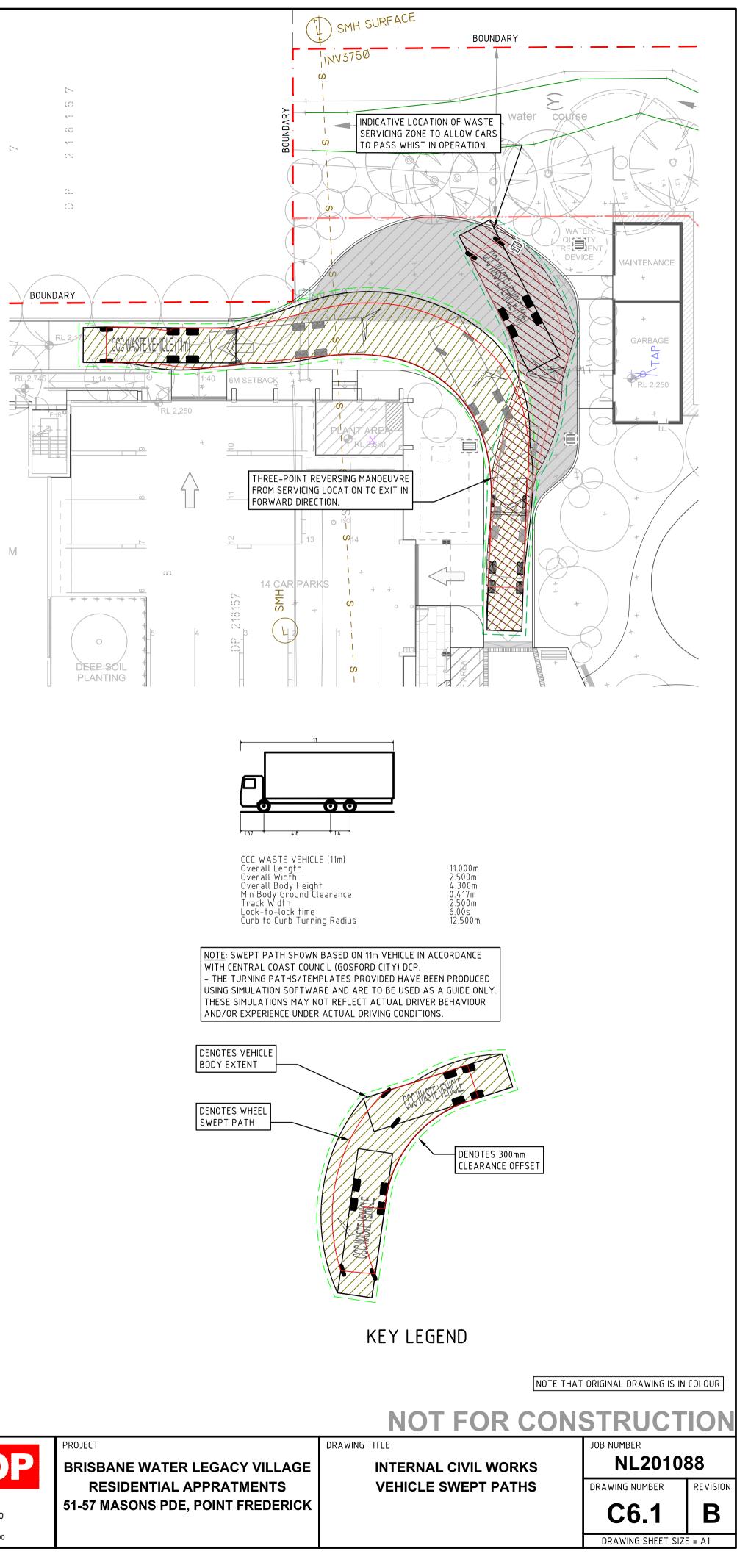
NOTE THAT ORIGINAL DRAWING IS IN COLOUR

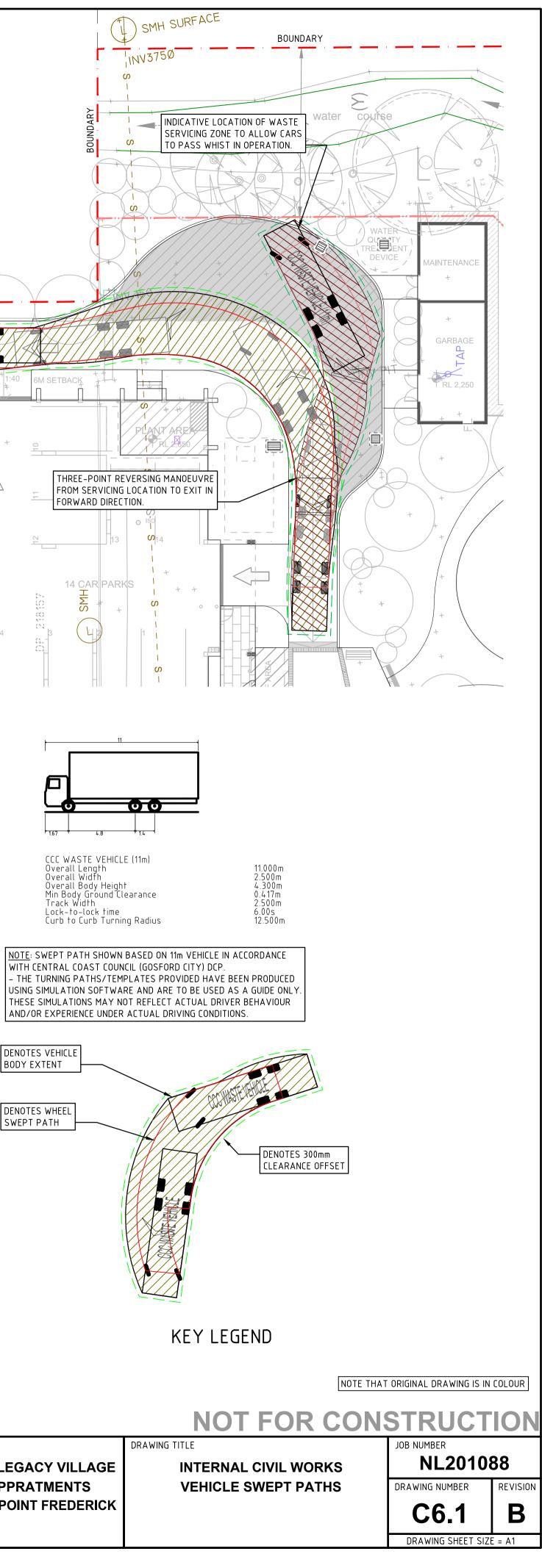


LEGACY VILLAGE APPRATMENTS , POINT FREDERICK

DRAWING TITLE INTERNAL CIVIL WORKS LONG SECTIONS & CROSS SECTIONS SHEET 1 JOB NUMBER
NL201088
DRAWING NUMBER
C5.1
B
DRAWING SHEET SIZE = A1









MUSIC-*link* Report

Project Details		Company De	tails
Project:	NL201088 51-57 Masons Parade	Company:	Northrop Consulting Engineers
Report Export Date:	10/09/2021	Contact:	Robert Suckling
Catchment Name:	NL201088 DA Issue_RS	Address:	Suite 4, 257-259 Central Cost Highway, Erina
Catchment Area:	0.608ha	Phone:	02 4365 1668
Impervious Area*:	61.91%	Email:	rsuckling@northrop.com.au
Rainfall Station:	66062 SYDNEY		
Modelling Time-step:	6 Minutes		
Modelling Period:	1/01/1974 - 31/12/1993 11:54:00 PM		
Mean Annual Rainfall:	1297mm		
Evapotranspiration:	1261mm		
MUSIC Version:	6.3.0		
MUSIC-link data Version:	6.33		
Study Area:	Lowland		
Scenario:	Central Coast Development		

* takes into account area from all source nodes that link to the chosen reporting node, excluding Import Data Nodes

Treatment Train Effectiveness		Treatment Nodes		Source Nodes	
Node: Post-Development Node	Reduction	Node Type	Number	Node Type	Number
Row	30.5%	Rain Water Tank Node	1	Urban Source Node	6
TSS	80.7%	Sedimentation Basin Node	1		
TP	63.2%	Buffer Node	1		
TN	54.5%	GPT Node	1		
GP	91.1%	Generic Node	1		

Comments

Parameters reflective of precast chamber.



Passing Parameters

Node Type	Node Name	Parameter	Min	Max	Actual
Buffer	Buffer	Proportion of upstream impervious area treated	None	None	1
GPT	7 x OceanGuard200um	Hi-flow bypass rate (cum/sec)	None	99	0.14
Post	Post-Development Node	% Load Reduction	None	None	30.5
Post	Post-Development Node	GP % Load Reduction	90	None	91.1
Post	Post-Development Node	TN % Load Reduction	45	None	54.5
Post	Post-Development Node	TP % Load Reduction	45	None	63.2
Post	Post-Development Node	TSS % Load Reduction	80	None	80.7
Sedimentation	SF Manhole DN2250 (1.6m2)	Exfiltration Rate (mm/hr)	0	0	0
Sedimentation	SF Manhole DN2250 (1.6m2)	Extended detention depth (m)	0.25	1	0.77
Sedimentation	SF Manhole DN2250 (1.6m2)	High Flow Bypass Out (ML/yr)	None	None	0
Urban	Building Podium 0.017ha. 50% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Building Podium 0.017ha. 50% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Building Podium 0.017ha. 50% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Building Podium 0.017ha. 50% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Building Podium 0.017ha. 50% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.6	-0.6	-0.6
Urban	Building Podium 0.017ha. 50% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.15	2.15	2.15
Urban	Carpark 0.153ha 100% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Carpark 0.153ha 100% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Carpark 0.153ha 100% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Carpark 0.153ha 100% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.34	0.34	0.34
Urban	Carpark 0.153ha 100% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.3	-0.3	-0.3
Urban	Carpark 0.153ha 100% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.43	2.43	2.43
Urban	Driveway By-Pass 0.024ha 100% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Driveway By-Pass 0.024ha 100% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Driveway By-Pass 0.024ha 100% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Driveway By-Pass 0.024ha 100% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.34	0.34	0.34
Urban	Driveway By-Pass 0.024ha 100% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.3	-0.3	-0.3
Urban	Driveway By-Pass 0.024ha 100% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.43	2.43	2.43
Urban	Landscape 0.042ha. 0% Imp	Baseflow Total Nitrogen Mean (log mg/L)	-0.05	-0.05	-0.05
Urban	Landscape 0.042ha. 0% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-1.22	-1.22	-1.22
Urban	Landscape 0.042ha. 0% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.15	1.15	1.15
Urban	Landscape 0.042ha. 0% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Landscape 0.042ha. 0% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.66	-0.66	-0.66
Urban	Landscape 0.042ha. 0% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	1.95	1.95	1.95
Urban	Landscape 0.227 ha. 20% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Landscape 0.227 ha. 20% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Landscape 0.227 ha. 20% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Landscape 0.227 ha. 20% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Landscape 0.227 ha. 20% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.6	-0.6	-0.6
Urban	Landscape 0.227 ha. 20% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.15	2.15	2.15

Only certain parameters are reported when they pass validation

NOTE: A successful self-validation check of your model does not constitute an approved model by Central Coast Council MUSIC-*link* now in MUSIC by eWater – leading software for modelling stormwater solutions



Node Type	Node Name	Parameter	Min	Max	Actual
Urban	Roof 0.145ha. 100% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.32	0.32	0.32
Urban	Roof 0.145ha. 100% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.82	-0.82	-0.82
Urban	Roof 0.145ha. 100% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.1	1.1	1.1
Urban	Roof 0.145ha. 100% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Roof 0.145ha. 100% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.89	-0.89	-0.89
Urban	Roof 0.145ha. 100% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	1.3	1.3	1.3
Only contain name	motors are reported when they page	validation			

Only certain parameters are reported when they pass validation

NOTE: A successful self-validation check of your model does not constitute an approved model by Central Coast Council MUSIC-*link* now in MUSIC by eWater – leading software for modelling stormwater solutions



Failing Parameters

Node Type	Node Name	Parameter	Min	Max	Actual
Sedimentation	SF Manhole DN2250 (1.6m2)	Notional Detention Time (hrs)	8	12	0.0622
Sedimentation	SF Manhole DN2250 (1.6m2)	Total Nitrogen - k (m/yr)	500	500	1
Sedimentation	SF Manhole DN2250 (1.6m2)	Total Phosphorus - k (m/yr)	6000	6000	1
Sedimentation	SF Manhole DN2250 (1.6m2)	Total Suspended Solids - k (m/yr)	8000	8000	1
Only certain parameters	Only certain parameters are reported when they pass validation				

NOTE: A successful self-validation check of your model does not constitute an approved model by Central Coast Council MUSIC-*link* now in MUSIC by eWater – leading software for modelling stormwater solutions



26 March 2021

Dear Applicant,

I refer to your recent application for flood information. The information provided below is based on the available Council data at the time of application.

Property Details

Lot	51	DP	732632
Address	51-57 Masons Pde, Point Frederic	ck NSW 22	250

Calculated Flood Levels

Flood Level
3.52m AHD
2.37m AHD
2.10m AHD

Refer to glossary for definitions

The above flood levels represent the maximum flood level within the lot boundary. The flood data maps are attached in the appendix.

Source of Flooding information: Gosford CBD Local Overland Flood Study 2013, Brisbane Water Foreshore Flood Risk Management Study 2015

Minimum Floor Level (MFL)

The residential minimum floor level is **2.87m AHD**. The minimum floor level at this property is derived from the maximum 1% AEP Flood Level plus allowance for sea level rise plus 500mm freeboard. The minimum floor level may vary at different locations within the lot boundary.

State Environmental Planning Policy- SEPP (Exempt and Complying Development Codes) 2008

In accordance with State Environmental Planning Policy (Exempt and Complying Development Codes) 2008, if whole or part of the property is located within at least one of the exclusionary categories in Clause 3.5, development may not be permitted.

The table below contains hazard and hydraulic categorisation of the property in accordance with the NSW Floodplain Development Manual April 2005; Exclusionary categories listed in SEPP 2008, Clause 3.5

Hazard, Hydraulic, and SEPP 2008 exclusionary Categorisation

 Wyong Office: 2 Hely St / PO Box 20 Wyong NSW 2259

 Gosford Office: 49 Mann St / PO Box 21 Gosford NSW 2250

 P 1300 463 954 | E ask@centralcoast.nsw.gov.au | W centralcoast.nsw.gov.au | ABN 73 149 644 003

 Flood Information: 51-57 Masons Pde Pt Frederick



1% AEP flood hazard	□ H1
	⊠ H2
	\boxtimes H3 (Complying Development may not be permitted)
	H4 (Complying Development may not be permitted)
	H5 (Complying Development may not be permitted)
	H6 (Complying Development may not be permitted)
	□ N/A
Hydraulic categorisation	\boxtimes All or part of the property is located in a floodway (Complying
	Development may not be permitted)
	\boxtimes All or part of the property is located in a flood storage area
	(Complying Development may not be permitted)
	All or part of property is located in a flood fringe
	□ N/A
Exclusionary categories	Flood Storage Area
	🖾 Floodway Area
	Flow path
	High Hazard Area
	High Risk Area
	N/A (Complying Development may be permitted)

Disclaimer

Flood levels and minimum floor levels are provided in relation to Council's current records at the time of application. Council reserves the right to review and amend these levels from time to time. These amendments may impact the accuracy of information provided.



Glossary

AHD	Australian Height Datum is a common national surface level datum
PMF	approximately corresponding to mean sea level. The Probable Maximum Flood is the largest flood that could
	conceivably occur.
1% AEP flood	The 1% Annual Exceedance Probability flood has a 1% (1:100) probability of occurring in any given year. This flood is also known as 1 in 100, 100yr ARI or Q100.
2% AEP flood	The 2% Annual Exceedance Probability flood has a 2% (1:50) probability of occurring in any given year. This flood is also known as 1 in 50, 50yr ARI or Q50.
5% AEP flood	The 5% Annual Exceedance Probability flood has a 5% (1:20) probability of occurring in any given year. This flood is also known as 1 in 20, 20yr ARI or Q20.
H1 Hazard Categorisation*	Generally safe for people, vehicles and buildings
H2 Hazard Categorisation*	Unsafe for small vehicles
H3 Hazard Categorisation*	Unsafe for vehicles, children and the elderly
H4 Hazard Categorisation*	Unsafe for people and vehicles
H5 Hazard Categorisation*	Unsafe for vehicles and people. All buildings vulnerable to structural damage. Some less robust building types vulnerable to failure
H6 Hazard Categorisation*	Unsafe for vehicles and people. All building types considered vulnerable to failure
Floodways*	Those areas where a significant volume of water flows during floods and are often aligned with obvious natural channels. They are areas that, even if only partially blocked, would cause a significant increase in flood levels and/or a significant redistribution of flood flow, which may in turn adversely affect other areas. They are often, but not necessarily, areas with deeper flow or areas where higher velocities occur.
Flood storage*	Those parts of the floodplain that are important for the temporary storage of floodwaters during the passage of flood. If the capacity of a flood storage area is substantially reduced by, for example, the construction of levees or by landfill, flood levels in nearby areas may rise and the peak discharge downstream may be increased. Substantial reduction of the capacity of a flood storage area can also cause a significant redistribution of flood flows.
Flood fringe*	The remaining area of land affected by flooding, after floodway and flood storage areas have been defined.

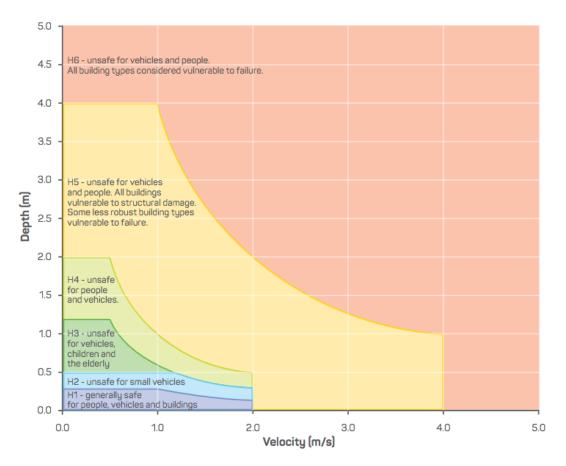
Source – NSW Floodplain Development Manual April 2005

Hydraulic Hazard AIDR ref <u>https://knowledge.aidr.org.au/media/3518/adr-guideline-7-3.pdf</u>

NSW FDM ref <u>https://www.environment.nsw.gov.au/topics/water/floodplains/floodplain-</u> manual







Source – Australian Institute for Disaster Resilience 2017. Hydraulic Hazard: refer also to Australian Rainfall and Runoff Section 7.2.7 General Flood Hazard Curves (Figure 6.7.9) <u>http://book.arr.org.au.s3-website-ap-southeast-2.amazonaws.com/</u>

The information provided in this letter is provided only to you and is not intended to be provided to a third party.

Should you have any enquiries concerning this letter, please do not hesitate to contact Andrew Dewar on 1300 463 954 during the hours of 8.30am to 5.00pm Monday to Friday.

Yours faithfully,

Andrew Dewar Floodplain Development Engineer

Phone: 1300 463 954



<u>Appendix</u>

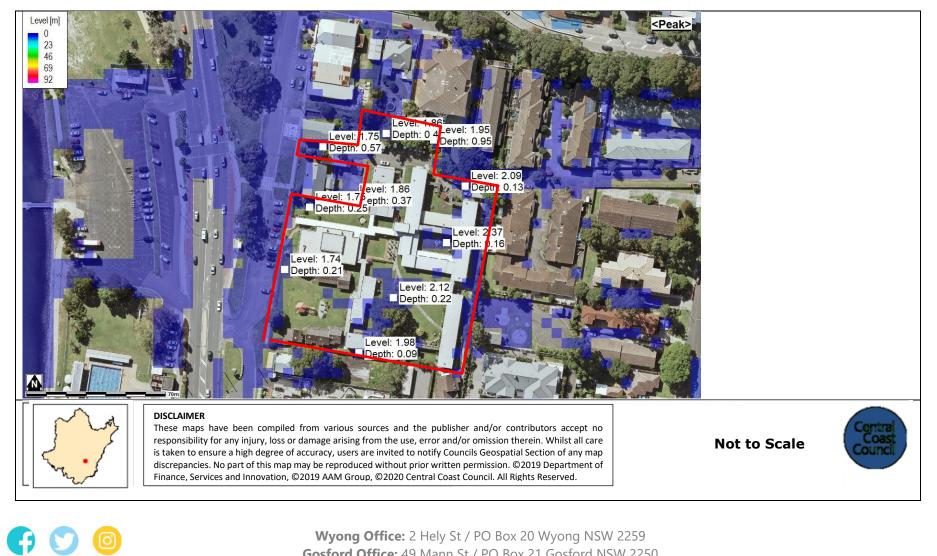
PMF Flood Extent



Flood Information: 51-57 Masons Pde Pt Frederick



1% AEP Flood Extent



Wyong Office: 2 Hely St / PO Box 20 Wyong NSW 2259Gosford Office: 49 Mann St / PO Box 21 Gosford NSW 2250P 1300 463 954 | E ask@centralcoast.nsw.gov.au | W centralcoast.nsw.gov.au | ABN 73 149 644 003Flood Information: 51-57 Masons Pde Pt FrederickPage | 6



5% AEP Flood Extents

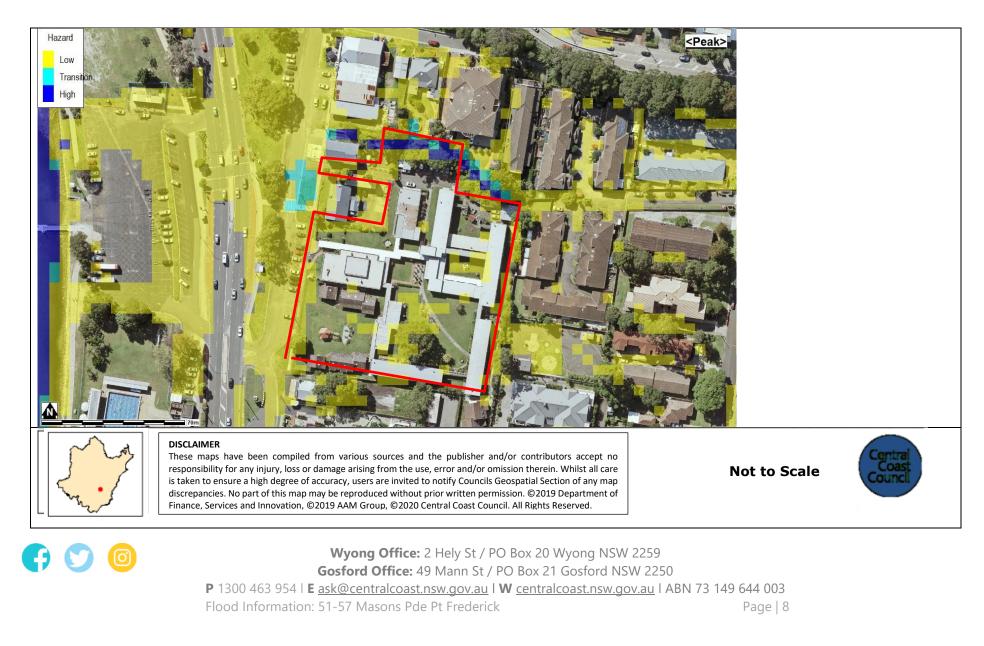


Flood Information: 51-57 Masons Pde Pt Frederick

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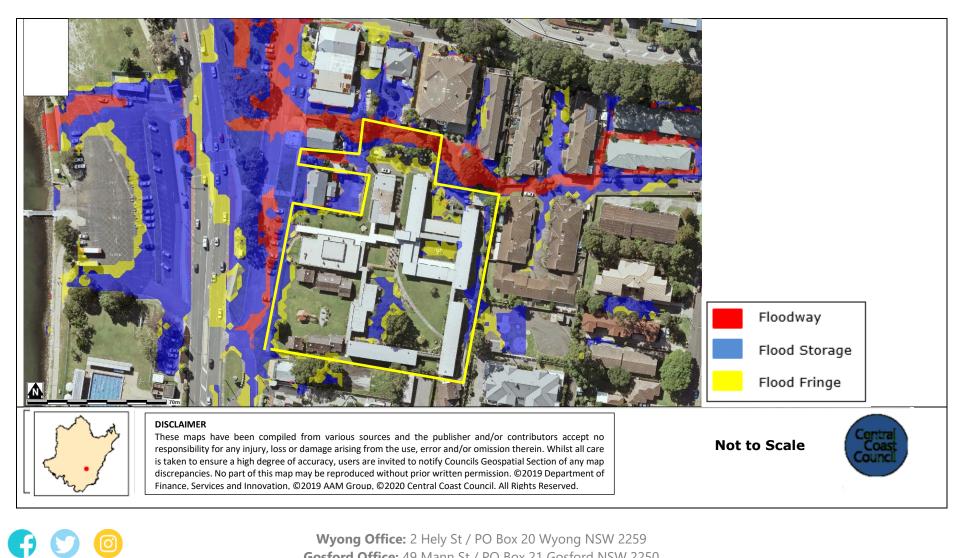


Hazard Categorisation





Hydraulic Categorisation



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BRISBANE WATER LEGACY VILLAGE RESIDENTIAL APARTMENTS

51-57 MASONS PDE, POINT FREDERICK INTERNAL CIVIL WORKS



REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLIENT	ARCHITECT
А	DEVELOPMENT APPLICATION	КT		DH	21.05.21		INTEGRAT
В	DEVELOPMENT APPLICATION	КT		DH	15.09.21	Grindlev	
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DRAWING SCHEDULE

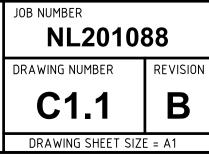
DWG No.	DRAWING TITLE
C1.1	COVER SHEET
C2.1	CONCEPT SEDIMENT & EROSION CONTROL PLAN
C2.2	SEDIMENT & EROSION CONTROL DETAILS
C4.1	STORMWATER MANAGEMENT & LEVELS PLAN
C5.1	LONG SECTIONS & CROSS SECTIONS – SHEET 1
C6.1	VEHICLE SWEPT PATHS

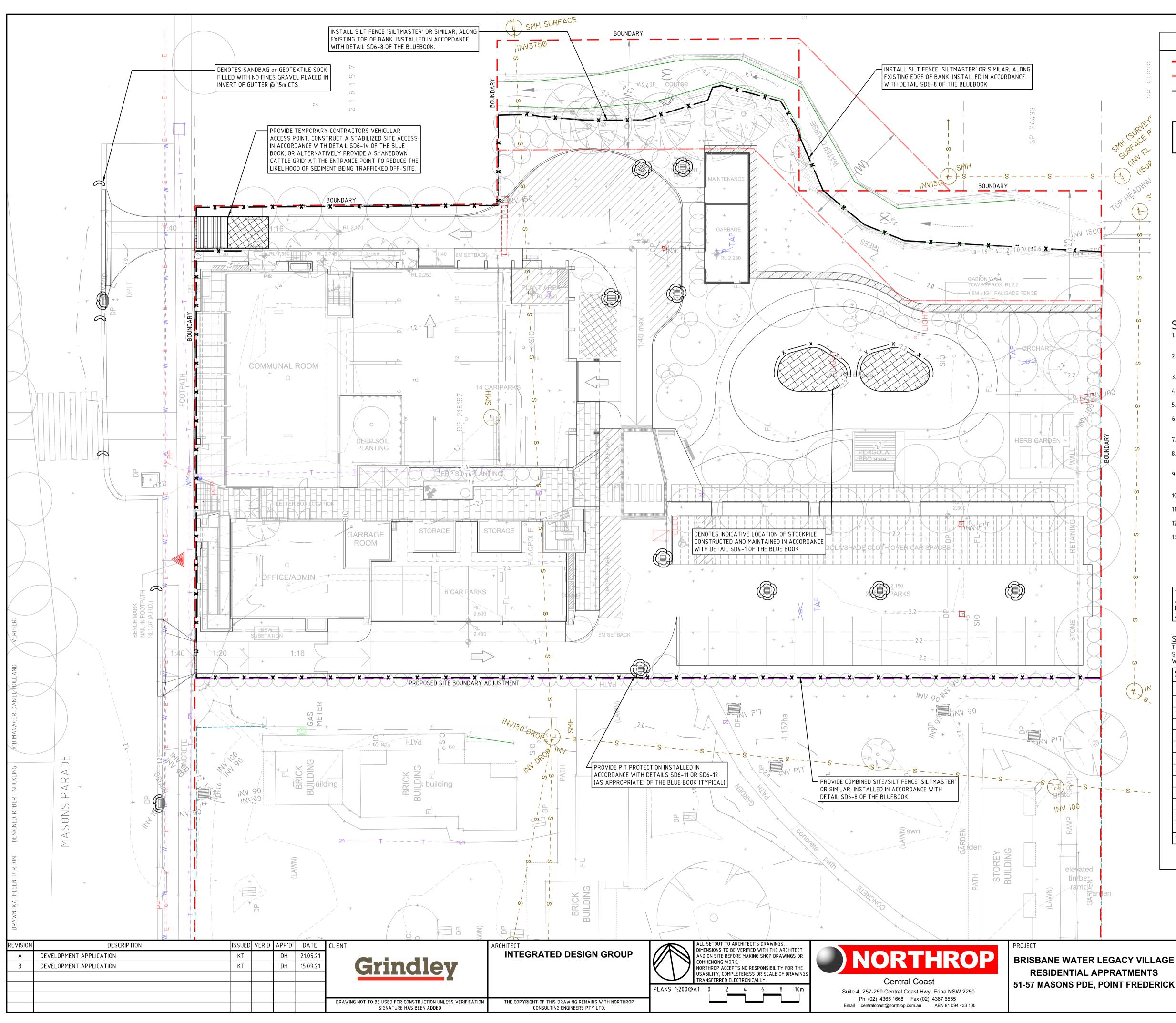
ATED DESIGN GROUP	ALL SETOUT TO ARCHITECT'S DRAWINGS, DIMENSIONS TO BE VERIFIED WITH THE ARCHITECT AND ON SITE BEFORE MAKING SHOP DRAWINGS OR COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS	NORTHROP	PROJECT BRISBANE WATER I RESIDENTIAL A	
	TRANSFERRED ELECTRONICALLY.	Central Coast	51-57 MASONS PDE, I	
		Suite 4, 257-259 Central Coast Hwy, Erina NSW 2250	51-57 WASONS FDE, I	
DF THIS DRAWING REMAINS WITH NORTHROP ISULTING ENGINEERS PTY LTD.		Ph (02) 4365 1668 Fax (02) 4367 6555 Email centralcoast@northrop.com.au ABN 81 094 433 100		

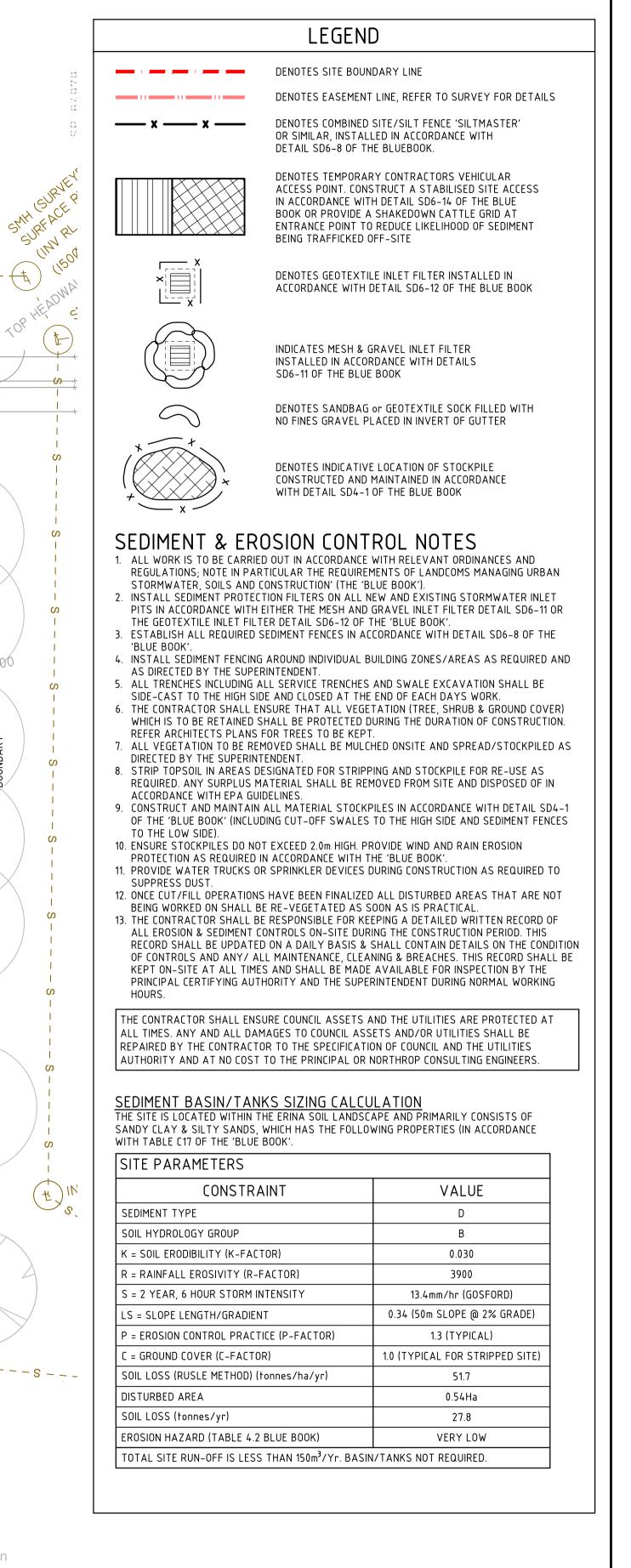


NOT FOR CONSTRUCTION DRAWING TITLE

LEGACY VILLAGE **APPRATMENTS** , POINT FREDERICK INTERNAL CIVIL WORKS **COVER SHEET**







NOTE THAT ORIGINAL DRAWING IS IN COLOUR

JOB NUMBER

DRAWING NUMBER

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DRAWING TITLE

INTERNAL CIVIL WORKS **CONCEPT SEDIMENT & EROSION** CONTROL PLAN

C2. Β DRAWING SHEET SIZE = A1

NL201088

REVISION

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLIENT	ARCHITECT
А	DEVELOPMENT APPLICATION	КT		DH	21.05.21		INTEGRATED DESIGN GROUP
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CONSTRUCTION NOTES

- 1. STRIP THE TOPSOIL, LEVEL THE SITE AND COMPACT THE SUBGRADE.

TO DIVERT WATER TO THE SEDIMENT FENCE.

- 2. COVER THE AREA WITH NEEDLE-PUNCHED GEOTEXTILE.

- 3. CONSTRUCT A 200mm THICK PAD OVER THE GEOTEXTILE USING ROAD BASE OR 30mm AGGREGATE.

- 4. ENSURE THE STRUCTURE IS AT LEAST 15 METRES LONG OR TO BUILDING ALIGNMENT AND AT LEAST 3 METRES
- WIDE. 5. WHERE A SEDIMENT FENCE JOINS ONTO THE STABILISED ACCESS, CONSTRUCT A HUMP IN THE STABILISED ACCESS

STABILISED SITE ACCESS (SD 6-14)

RUNOFF DIRECTED TO SEDIMENT TRAP/FENCE

> DGB 20 ROADBASE OR 30mm AGGREGATE ——

GEOTEXTILE FABRIC DESIGNED TO PREVENT

AND TO MAINTAIN GOOD PROPERTIES OF THE SUB-BASE LAYERS. GEOFABRIC MAY BE A WOVEN OR NEEDLE-PUNCHED PRODUCT WITH A MINIMUM CBR BURST STRENGTH (AS3706.4-90) OF 2500 N -----

INTERMIXING OF SUBGRADE AND BASE MATERIALS

CONSTRUCTION SITE

NOT SATISFACTORY.

SEDIMENT FENCE (SD 6-8)

MINIMUM WIDTH 3m

MINIMUM LENGTH 15m

EXISTING

ROADWAY -

2. CUT A 150mm DEEP TRENCH ALONG THE UPSLOPE LINE OF THE FENCE FOR THE BOTTOM OF THE FABRIC TO BE ENTRENCHED. DRIVE 1.5 METRE LONG STAR PICKETS INTO GROUND AT 2.5 METRE INTERVALS (MAX) AT THE DOWNSLOPE EDGE 3. OF THE TRENCH. ENSURE ANY STAR PICKETS ARE FITTED WITH SAFETY CAPS.

THE TRENCH. FIX THE GEOTEXTILE WITH WIRE TIES OR AS RECOMMENDED BY THE MANUFACTURER. ONLY USE

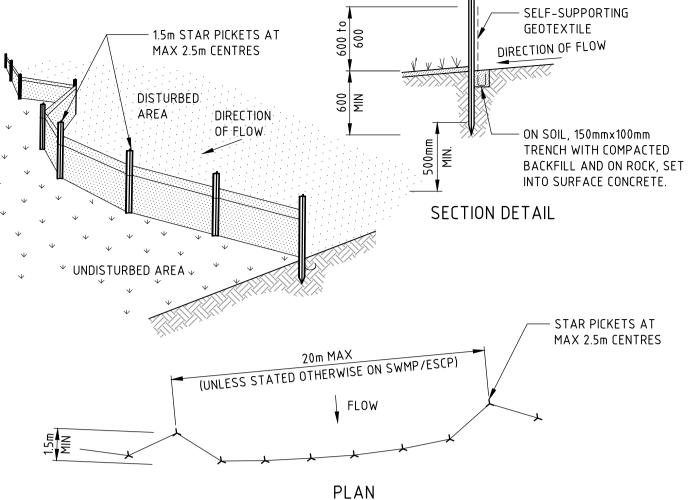
GEOTEXTILE SPECIFICALLY PRODUCED FOR SEDIMENT FENCING. THE USE OF SHADE CLOTH FOR THIS PURPOSE IS

4. FIX SELF-SUPPORTING GEOTEXTILE TO THE UPSLOPE SIDE OF THE POSTS ENSURING IT GOES TO THE BASE OF

6. BACKFILL THE TRENCH OVER THE BASE OF THE FABRIC AND COMPACT IT THOROUGHLY OVER THE GEOTEXTILE.

5. JOIN SECTIONS OF FABRIC AT A SUPPORT POST WITH A 150mm OVERLAP.

- 50 LITRES PER SECOND IN THE DESIGN STORM EVENT, USUALLY THE 10-YEAR EVENT.
- THE CATCHMENT AREA SHOULD BE SMALL ENOUGH TO LIMIT WATER FLOW IF CONCENTRATED AT ONE POINT TO
- CONSTRUCTION NOTES CONSTRUCT SEDIMENT FENCES AS CLOSE AS POSSIBLE TO BEING PARALLEL TO THE CONTOURS OF THE SITE, BUT WITH SMALL RETURNS AS SHOWN IN THE DRAWING TO LIMIT THE CATCHMENT AREA OF ANY ONE SECTION.



1.5m STAR PICKETS AT MAX 2.5m CENTRES

PROPERTY

BOUNDARY

-	тыс			WITH	NORTHROP	
	ппэ	DRAWING	REMAINS	WIIII	NUKINKUP	
sι	JLTIN	G ENGINEE	RS PTY L	TD.		

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PROJECT **BRISBANE WATER LEGACY VILLAGE RESIDENTIAL APPRATMENTS** 51-57 MASONS PDE, POINT FREDERICK

OR SWMP TO REDUCE THE C-FACTOR TO LESS THAN 0.10. 5. CONSTRUCT EARTH BANKS (STANDARD DRAWING 5-5) ON THE UPSLOPE SIDE TO DIVERT WATER AROUND

4. WHERE THEY ARE TO BE IN PLACE FOR MORE THAN 10 DAYS, STABILISE FOLLOWING THE APPROVED ESCP

STOCKPILES (SD 4-1)

- 3. WHERE THERE IS SUFFICIENT AREA, TOPSOIL STOCKPILES SHALL BE LESS THAN 2m IN HEIGHT.
- 2. CONSTRUCT ON THE CONTOUR AS LOW, FLAT, ELONGATED MOUNDS.

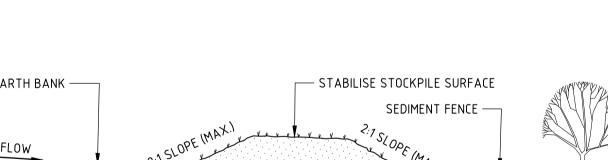
STOCKPILES AND SEDIMENT FENCES (STANDARD DRAWING 6-8) 1 TO 2m DOWNSLOPE.

- FLOW, ROADS AND HAZARD AREAS.

- 1. PLACE STOCKPILES MORE THAN 2m (PREFERABLY 5m) FROM EXISTING VEGETATION, CONCENTRATED WATER

- CONSTRUCTION NOTES

EARTH BANK ———	STABILISE STOCKPILE SURFACE	WW SPELL
	SEDIMENT FENCE	
FLOW	21 SLOPE (MAX)	
- XININI TANU XINI T		



- KERB-SIDE INLET

GRAVEL-FILLED WIRE MESH

OR GEOTEXTILE 'SAUSAGE'

AND FILL IT WITH 25mm TO 50mm GRAVEL. 4. PLACE THE FILTER AT THE OPENING LEAVING AT LEAST A 100mm SPACE BETWEEN IT AND THE KERB INLET.

PLACED SO THAT THEY FIRMLY ABUT EACH OTHER AND SEDIMENT-LADEN WATERS CANNOT PASS BETWEEN.

MESH AND GRAVEL INLET FILTER (SD 6-11)

- 3. FORM AN ELLIPTICAL CROSS-SECTION ABOUT 150mm HIGH x 400mm WIDE.
- 2. FABRICATE A SLEEVE MADE FROM GEOTEXTILE OR WIRE MESH LONGER THAN THE LENGTH OF THE INLET PIT
- 1. INSTALL FILTERS TO KERB INLETS ONLY AT SAG POINTS.

6. SANDBAGS FILLED WITH GRAVEL CAN SUBSTITUTE FOR THE MESH OR GEOTEXTILE PROVIDING THEY ARE

– OVERFLOW

TIMBER SPACER TO SUIT

- CONSTRUCTION NOTES





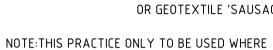
5. FORM A SEAL WITH THE KERB TO PREVENT SEDIMENT BYPASSING THE FILTER.

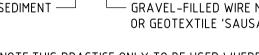
TIMBER SPACER TO SUIT.

RUNOFF WATER WITH

MAINTAIN THE OPENING WITH SPACER BLOCKS.

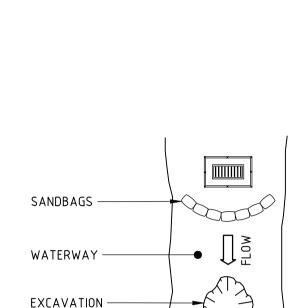
SEDIMENT.











STAR PICKETS —

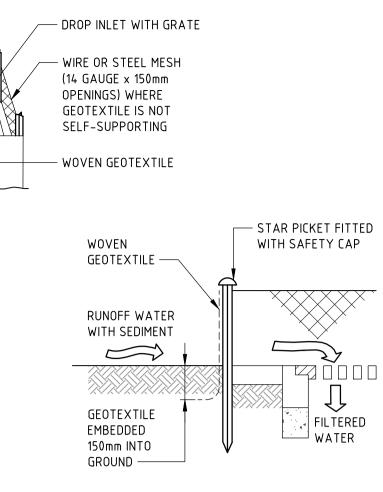
1 METRE MAX.

EXCAVATION -

EARTH BANK

CONSTRUCTION NOTES

- 1. FABRICATE A SEDIMENT BARRIER MADE FROM GEOTEXTILE OR STRAW BALES.
- STRAW BALES OR GEOFABRIC. REDUCE THE PICKET SPACING TO 1 METRE CENTRES.
- 3. IN WATERWAYS, ARTIFICIAL SAG POINTS CAN BE CREATED WITH SANDBAGS OR EARTH BANKS AS SHOWN IN
- THE DRAWING.
- TO BYPASS IT.



FOR DROP INLETS AT NON-SAG POINTS, SANDBAGS, EARTH BANK OR EXCAVATION USED TO CREATE ARTIFICIAL SAG POINT

2. FOLLOW STANDARD DRAWING 6-7 AND STANDARD DRAWING 6-8 FOR INSTALLATION PROCEDURES FOR THE

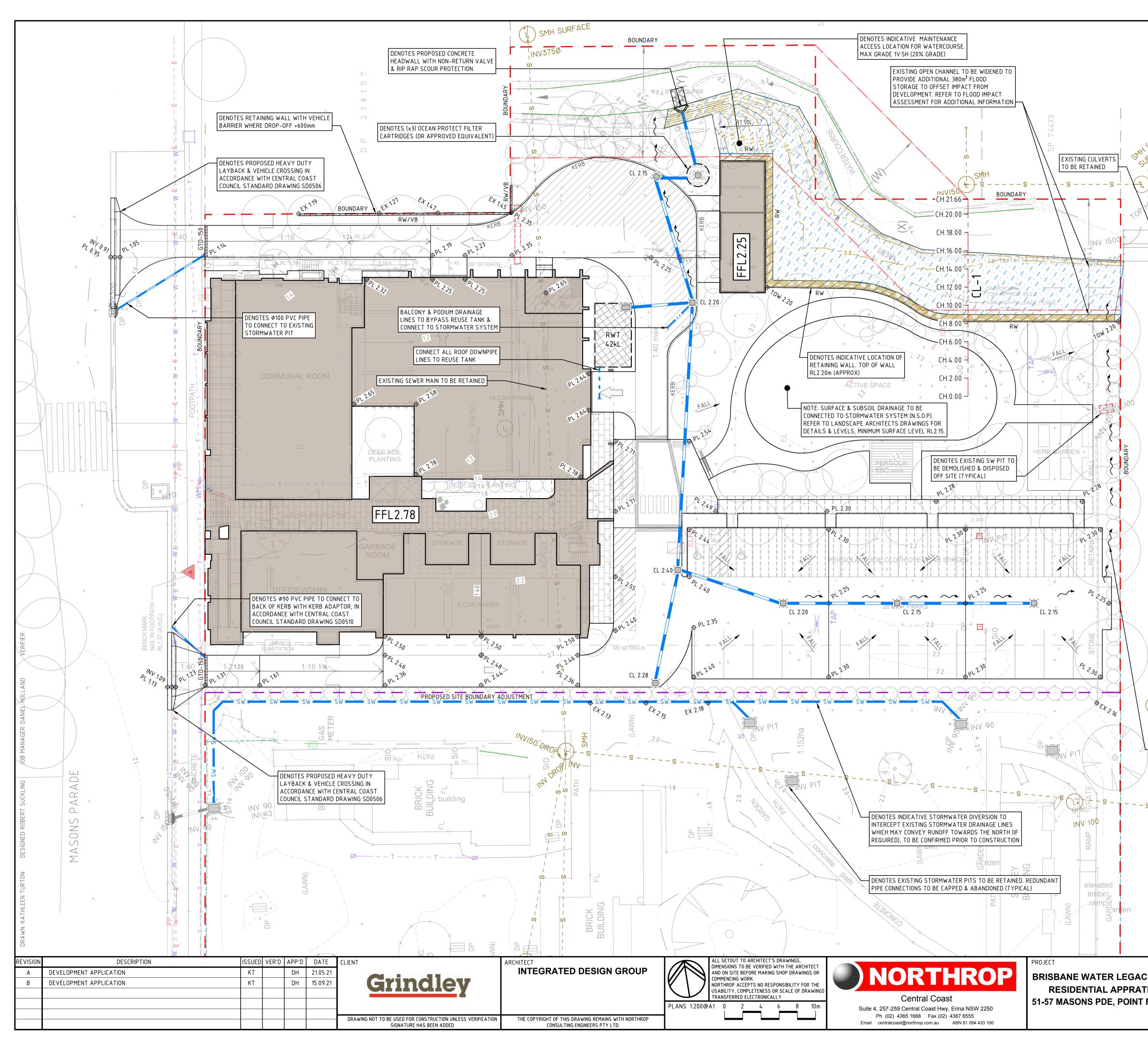
4. DO NOT COVER THE INLET WITH GEOTEXTILE UNLESS THE DESIGN IS ADEQUATE TO ALLOW FOR ALL WATERS

GEOTEXTILE INLET FILTER (SD 6–12)

NOT FOR CONSTRUCTION DRAWING TITLE

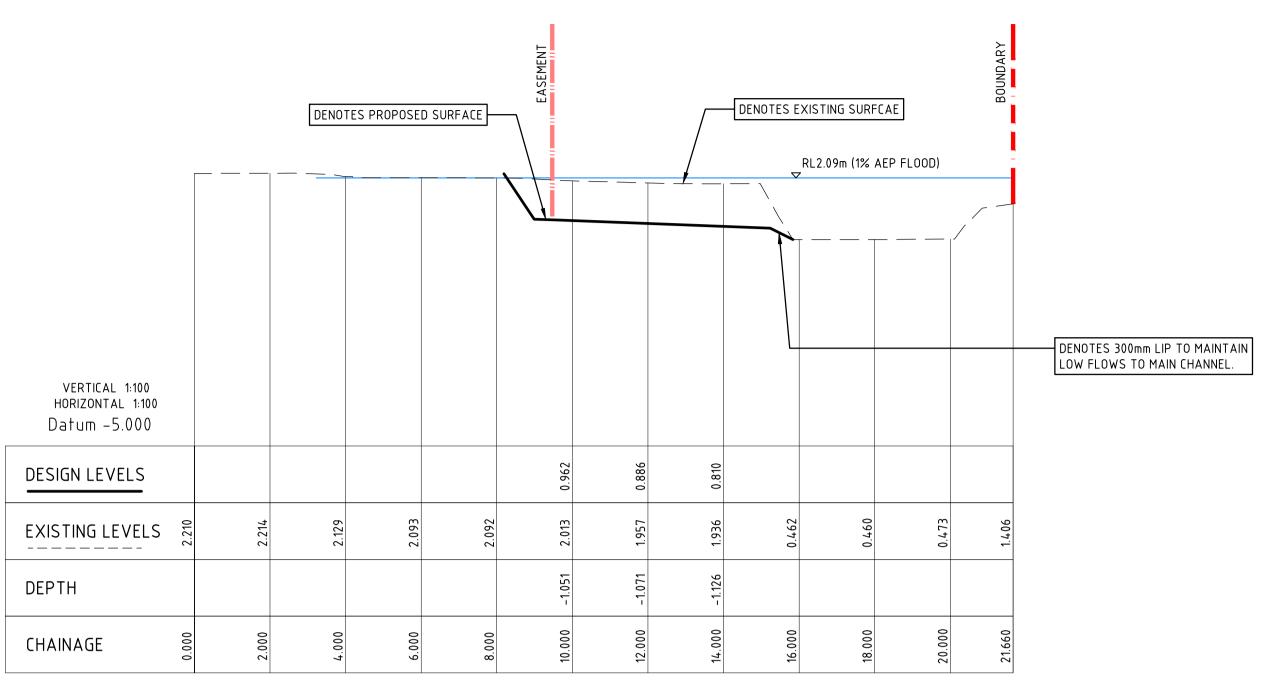
INTERNAL CIVIL WORKS **SEDIMENT & EROSION** CONTROL DETAILS

JOB NUMBER NL201088 DRAWING NUMBER REVISION Β UZ. DRAWING SHEET SIZE = A1



		LEGEND		
707		DENOTES SITE BOUNDARY LINE		
		DENOTES EASEMENT LINE, REFER	TENTS, REFER TO	Ì
	FFL2.78	ARCHITECTURAL & STRUCTURAL DENOTES PROPOSED FINISHED FLU		
SURVEY REACE P				
2FA RL	+ ^{PL L.}	DENOTES PROPOSED FINISHED SU		
UNN USOG	$ \begin{array}{c} \oplus PL^{2,30} \\ \oplus UL^{2,15} \\ \oplus EX^{2,15} \end{array} $	DENOTES PROPOSED STORMWATE		
LEADWA	⊕ ^{∠¹}	DENOTES EXISTING CONTOURS		
	-10	DENOTES EXISTING CONTOURS		
CH0.00				
	CL-1	DENOTES ALIGNMENT CONTROL LI REFER TO LONG SECTION	NE & CHAINAGE,	
		DENOTES PROPOSED STORMWATE INLET PITS ARE TO BE FITTED WI ACCORDANCE WITH MANUFACTUR DENOTES EXISTING STORMWATEF BE RETAINED	TH FILTER INSERTS IN ERS SPECIFICATION	
	GTD-150	DENOTES GRATED TRENCH DRAIN	& WIDTH	
 		DENOTES CONCRETE HEADWALL W AND RIP RAP SCOUR PROTECTION		:
	RWT	DENOTES BELOW GROUND RAINWA COMBINED CAPACITY. HARVESTED FOR IRRIGATION & TOILET FLUSHI	D RAINWATER TO BE USED	
 	\mathbf{V}	DENOTES PROPOSED STORMWATE DENOTES OVERLAND FLOW PATH		
	RW/VB	DENOTES RETAINING WALL WITH (REQUIRED FOR DROP-OFFS GREA		
ν 	—— — — E — — ——	DENOTES APPROXIMATE LOCATIO ELECTRICITY LINE	N OF EXISTING	
-	——————————————————————————————————————	DENOTES APPROXIMATE LOCATIO	N OF EXISTING GAS MAIN	
	T	DENOTES APPROXIMATE LOCATIO TELECOMMUNICATION LINE	N OF EXISTING	
	W	DENOTES APPROXIMATE LOCATIO	N OF EXISTING WATER M	AIN
	S			
B	UILDER IS RESPONSIBLE FOR L	ES ARE APPROXIMATE ONLY & MA OCATING EXISTING INFRASTRUCTU /ELS ETC) PRIOR TO COMMENCING C	RE (CULVERTS, PITS, PIPE	
		MODIFY ALL EXISTING SERVICE CO ITH THE RELEVANT AUTHORITIES F		<i>J</i>
		CONTROL IN ACCORDANCE WITH ST INCIL SPECIFICATIONS/REQUIREMEN		ORY
()	OTE: ALL LEVELS TO AUSTRAL L1.564	IAN HEIGHT DATUM (AHD). ORIGIN	OF LEVELS PM 19217,	
	RAWINGS TO BE READ IN	CONJUNCTION WITH CONCEPT	STORMWATER	
	IANAGLMENT REPORT & T	LOOD IMPACT ASSESSMENT		
	DENOTES INDICATIVE OVERLAN PATH TO BE FREE OF OBSTRU(
5				
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Y VILLAGE		CIVIL WORKS	NL2010	88
MENTS FREDERICK		ER MANAGEMENT ELS PLAN	DRAWING NUMBER	REVISION
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DRAWING SHEET SIZE = A1



CL-1 FLOOD OFFSET STORAGE SECTION

REVISION A B	DESCRIPTION DEVELOPMENT APPLICATION DEVELOPMENT APPLICATION	ISSUED VER'D APP'D DATE KT DH 21.05.21 KT DH 15.09.21 Image: State S		ARCHITECT INTEGRATED DESIGN GROUP	ALL SETOUT TO ARCHITECT'S DRAWINGS, DIMENSIONS TO BE VERIFIED WITH THE ARCHITECT AND ON SITE BEFORE MAKING SHOP DRAWINGS OR COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED ELECTRONICALLY.	NORTHROP	PROJECT BRISBANE WATER LEC RESIDENTIAL APPI 51-57 MASONS PDE, PO
					Suite 4, 257-259 Central Coast Hwy, Erina NSW 2250 Ph (02) 4365 1668 Fax (02) 4367 6555 Email centralcoast@northrop.com.au ABN 81 094 433 100		

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LEGACY VILLAGE APPRATMENTS , POINT FREDERICK

DRAWING TITLE INTERNAL CIVIL WORKS LONG SECTIONS & CROSS SECTIONS SHEET 1 JOB NUMBER
NL201088
DRAWING NUMBER
C5.1
B
DRAWING SHEET SIZE = A1