

Northrop Consulting Engineers has been engaged by Grindley Pty Ltd to undertake conceptual civil and stormwater design and documentation for the development of the proposed Brisbane Water Legacy Village Residential Apartments at 51-57 Masons Parade, Point Frederick. This report accompanies, and should be read in conjunction with, drawings NL201088 C1.1 – C6.1.

We note the information contained in this report is not intended to present detailed design solutions but rather provide solutions commensurate with a conceptual design suitable for Development Application assessment.

The subject site is bounded by a multi-storey residential developments to the north, east and south; and Masons Parade to the west.

Figure 1 presents an aerial overview of the site.



- ## 4.2 WATER CONSERVATION

- Using water efficient fixtures for shower heads, toilet cisterns, toilet taps and kitchen taps including undertaking regular maintenance of these fixtures;
- The use of water efficient dishwashers;
- Landscaping with plant species that require minimal watering and irrigation with appropriate systems to minimise water loss and evaporation. This includes native plant species, using mulch around garden beds, avoiding watering when it's windy, watering during the coolest parts of the day and using drip irrigation;
- Harvested rainwater from part of the roof is proposed to be collected and reused for hardstand washdown, carwash bay and irrigation of landscaping areas.

4.2 RETENTION

- Quantity - the annual volume of stormwater reaching natural creeks and waterways;
- Rate - the peak flow rates leaving the site; and
- Response - the time it takes for rain to runoff the site.

The depth of stormwater runoff that must be captured by the stormwater source controls in order to achieve frequent discharge mitigation is termed the mitigation depth. The mitigation depth for various soil types and are shown below in Table 1.

Table 1: Mitigation Depth

Soil Texture	Mitigation Depth (mm)
Sand	14
Sandy Loam	14
Clay Loam	10
Clay	7

Based on geotechnical investigations performed on site, a clay soil profile is considered to best represent the soils to be encountered on site.

The volume of stormwater runoff that must be captured by a source control to achieve frequent discharge mitigation relative to the impervious surfaces that drain to the control is referred to as the mitigation storage and is calculated as shown below:

$$MS = (MIC \times MD) / 1000$$

where: MS = mitigation storage (m^3)

MIC = managed impervious catchment (m^2)

$$MD = \text{mitigation depth (mm)}$$

Using this method, the following mitigation storage for the impervious areas of the proposed development is calculated as shown below:

Mitigation depth	= 7mm	(clay soil type)
Mitigation area	= 3 720 m ²	(62% impervious)
Mitigation Storage	= [(3 720) x 7] / 1 000	
	= 26 m ³	

Using this method, the total mitigation storage, or retention storage required is 26 m³. It is proposed that a roof area of 1450 m² will drain to the below ground reuse tank with a total of 42kL storage capacity. The additional storage capacity provided will ensure that there is suitable reuse volume provided to meet the demand of the project. The reuse is proposed to be used for irrigation and hardstand washdown.

To ensure that there is adequate draw down, a MUSIC model was used to assess the efficiency of the reuse tank.

The assumed water usage rates are outlined as follows;

- Irrigation usage = 1 L/m²/day (NSW modelling guidelines)

The reuse tank demand and efficiency are outlined below.

Table 2 – Reuse Tank Demands

Reuse Tank	Tank size	Reuse Demand	Reuse Efficiency	Irrigation Area
Tank 1	42 kL	2.28 kL/Day	79.13%	2 280 m ²

As can be seen from Table 2, adequate draw down can be achieved based on the proposed tank sizing and reuse scheme.

[illegible][illegible][illegible][illegible]

Electrical Environmental Civil Hydraulic Mechanical Structural Electrical Environmental Civil Hydraulic Mechanical Structural Environmental
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Electrical Environmental Civil Hydraulic Mechanical Structural Electrical Environmental Civil Hydraulic Mechanical Structural

Civil Hydraulic Mechanical Structural Electrical Environmental Civil Hydraulic Mechanical Structural Electrical Environmental

[illegible]

- Civil Hydraulic Mechanical Structural Electrical Environmental Civil Hydraulic Mechanical Structural Electrical Environmental**

- Source node have been adopted from the NSW MUSIC Modelling Guideline (BMT WBM, 2015). Proprietary treatment nodes have been adopted from SPEL and Ocean Protect. The MUSIC modelling results for the above-mentioned treatment strategy are shown below in Table 4:

Pollutant Criteria	Reduction Target (%)	Sources (kg/yr)	Residual Load (kg/yr)	Achieved Reduction (%)
Total Suspended Solids (TSS)	80	951	184	80.7
Total Phosphorous (TP)	45	1.82	0.672	63.2
Total Nitrogen (TN)	45	11.4	5.2	54.5
Gross Pollutants	90	120	10.7	91.1

Table 4 shows that the proposed stormwater quality management strategy will achieve the required load reduction targets. A copy of the MUSIC Link report has been appended to the rear of this report.

The site is located immediately upstream of the local catchment outlet to Brisbane Water. Providing onsite detention for sites in the lower third of a catchment can have detrimental impacts to the peak discharge from the catchment as providing detention has the potential to delay the peak flow leaving the site and coinciding with the larger peak of the upstream catchment.

An overland flow path has been provided within the site to convey excess stormwater runoff towards the northern open channel via the internal circulation road.

The site is impacted by two separate flood events, the first being the overland surface flow generated from the upstream catchment and the second being foreshore flooding from the Brisbane Water foreshore.

Figure 3 presents the 1% AEP peak flood depths for the site as extracted from the Flood Information Certificate provided by Central Coast Council. It is noted that the flood behaviour observed is reflective of the Gosford CBD Local Overland Flow Flood Study prepared by Cardno (2013).

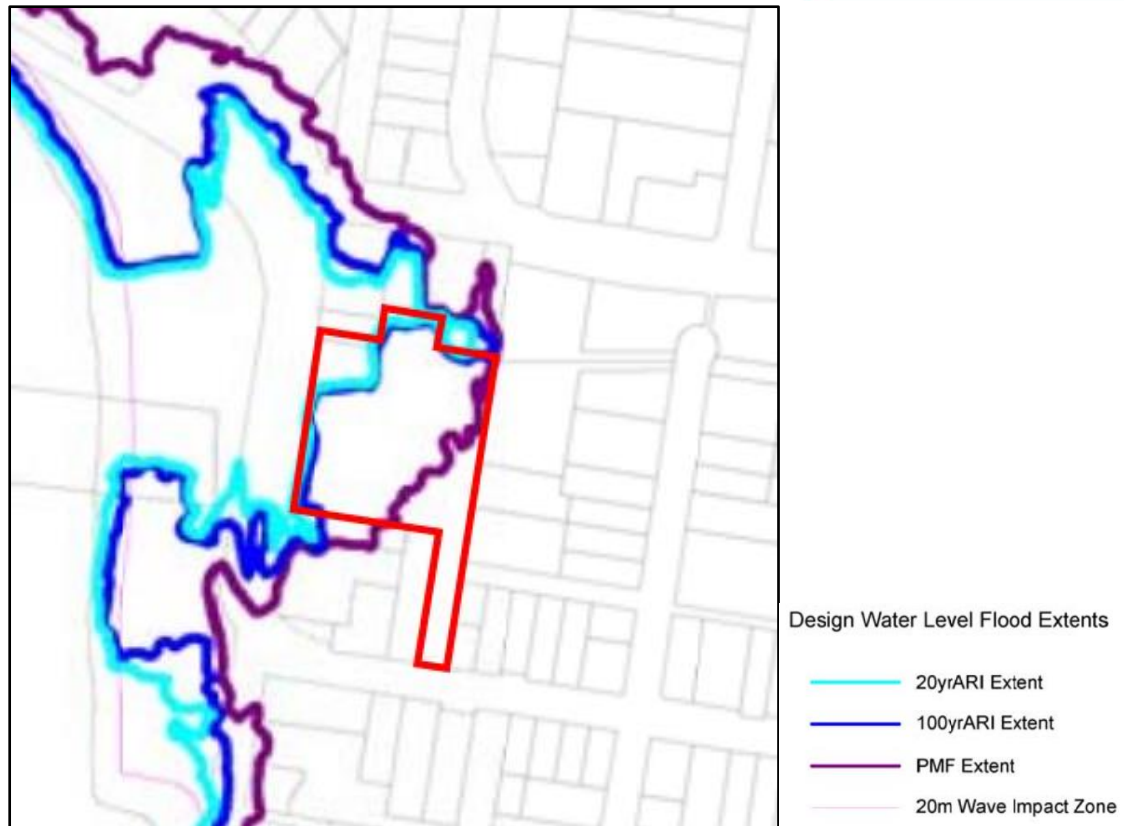


Figure 7 – Design Water Level Flood Extents (Cardno 2013 – Excerpt of Figure 6.16A)

It is observed that the site is only affected on the fringes of the site boundary in both the 5% and 1% AEP storm events. The PMF storm event is seen to inundate the majority of the site.

The flood levels were extracted from the flood study in the location of the subject site.

- 1% AEP = 1.71m AHD
- 1% AEP + 500mm freeboard = 2.21m AHD
- 1% AEP + 0.55m MSLR = 2.26m AHD
- PMF = 2.46m AHD

Flood Impacts - 1% AEP and PMF Flood Events

Figure 8 presents the building extents that was utilised for the Cardno overland flow study with the approximate proposed building extents overlayed. The existing building on the subject site are proposed to be demolished.

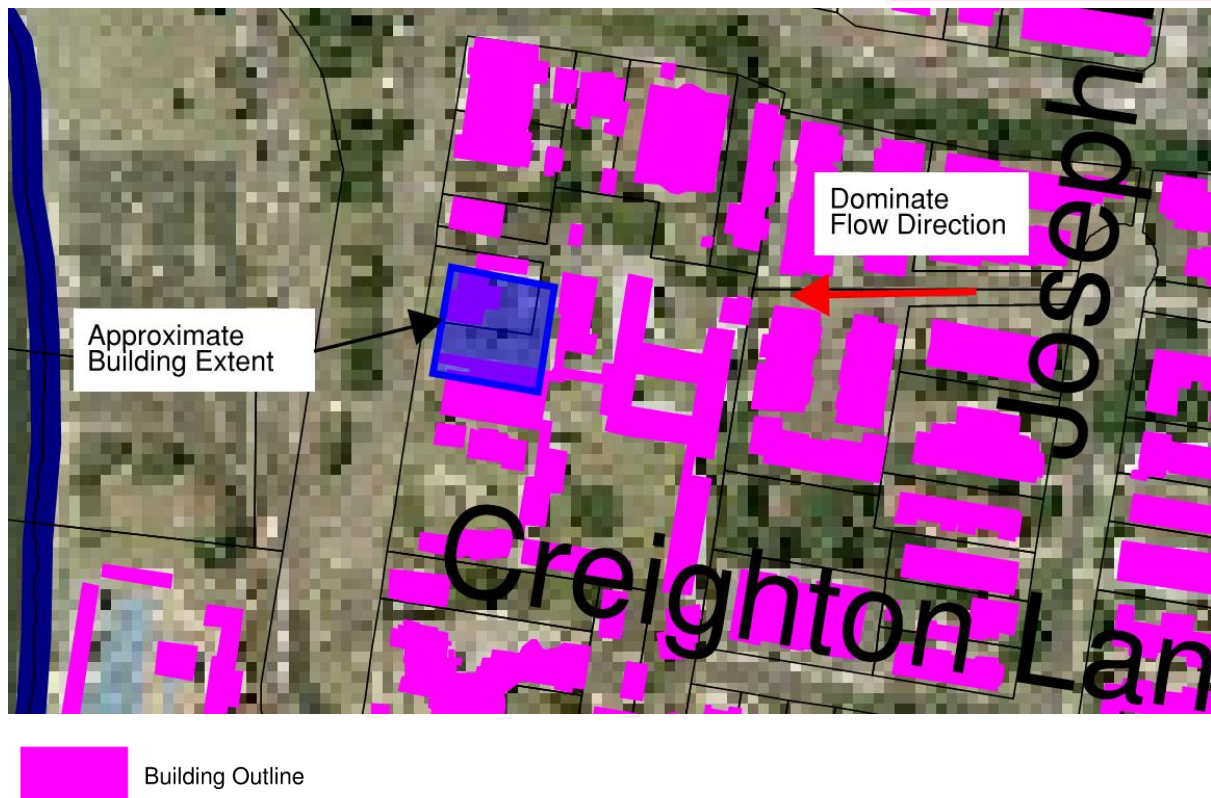


Figure 8 – Flood Model Obstructions (Cardno 2013 – Excerpt of Figure 3.5)

It can be observed that the proposed building extent is consistent or less than that currently adopted within the flood study. It can be reasonably determined, that when considering the flood impacts of the proposed development for the 1% AEP and PMF flood events, that the proposed development will not adversely affect the existing flood behaviour for the neighbouring properties. The proposed development may reduce the severity of flooding for surrounding properties as a number of existing buildings will be demolished and removed from the site, reducing the amount of blockage for any flows traversing through the site.

It is also noted that the effective cross-section for the open channel has not been reduced at any location through the site, and the proposed maintenance & garbage building is located outside of the existing 1% AEP flood extents.

Floor Levels

It is proposed that the floor levels of all habitable and non-habitable spaces are to be at or above the PMF level consistent with the controls for 'Seniors Housing'.

The floor level has been proposed to satisfy the highest flood level for the range of events including:

- Overland Flow:
 - 1% AEP + 500mm Freeboard = 2.36m AHD; or
 - PMF Event = **2.78m AHD**

Or

- Foreshore Flooding:
 - 1% AEP Flood Level + Sea Level Rise (50-year Design life) = 2.26m AHD; or
 - 1% AEP Flood Level + 500mm Freeboard = 2.21m AHD; or
 - PMF Flood Level = 2.46m AHD.

Note: Flood levels were obtained from the worst case levels within the footprint of the proposed development.

On-site refuge can be sought on-site during extreme flooding events, as the floor level of habitable and non-habitable spaces will be above the PMF level. Given the relatively short duration of the PMF flooding event, it is proposed that this is deemed acceptable, given the location of the site and surround flood hazards. Emergency access can be achieved towards the Central Coast Highway south of the site.

Earthworks & Site Filling

The site is identified to only contain small areas of flooding extent identified as flood storage, with the remaining areas classified as flood fringe, with the exception of the open channel north of the site.

It is proposed that the filling within the identified flooding extents shall be offset by providing the equivalent storage capacity elsewhere on-site, to ensure no significant adverse impacts on the flood behaviour for neighbouring and adjacent properties.

An 3D earthworks model was developed to compare the volume of storage lost by the proposed development, to the 1% flood level of 1.86m. It was calculated that 380m³ of potential flood storage would be lost due to the earthworks required to facilitate the development.

It is proposed that the existing open channel is locally widened to provide the 380m³ of offset flood storage required to mitigate any potential impacts.

The extent of filling required for the site when considering the potential flood impacts of the foreshore flooding event is deemed to have an inconsequential impact on the flood behaviour, given the relative volumes of fill compared to the volumes observed within the water body. Any filling will likely have an immeasurable and neglectable impact on surrounding flood levels.

Flood Summary

The flood characteristics of the site have been discussed, outlining the two major flood events that affect the proposed development. A review of Council's flood studies has been performed including discussion on the existing and proposed site impacts.

It has been demonstrated how the proposed development addresses the requirements of the Gosford DCP 2013, in particular Chapter 6.7 – Water Cycle Management (6.7.7.6 Flooding Targets). Discussion has been provided outlining the justification to not utilise an extensive 2D hydraulic flood model to demonstrate the flooding objectives can be achieved and instead provide qualitative assessment of the proposed development in conjunction with the previously prepared Flood Studies commissioned by Central Coast Council.

The proposed stormwater management design presented above has been prepared to comply with Central Coast Council (Gosford) DCP and Central Coast Council Design Guidelines as well as best industry practice. The design philosophy is based on the principle of at source treatment, to reduce conveyance infrastructure and manage water quantity and quality aspects.

R. Smith

D. Hall

Civil Engineer



REFERENCES:

Gosford Development Control Plan 2013

Central Coast Council, Civil Works Specification – Design Guideline 2018

BMT WBM Pty Ltd, New South Wales MUSIC Modelling Guidelines, August 2015

Central Coast Council, Water Sensitive Urban Design – Technical Guideline No 3. – Device Selection Guide, November 2010.

Gosford CBD Overland Flow Flood Study – Cardno 2013

Brisbane Water Foreshore Flood Study – Cardno 2013

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- Concept Stormwater Management Plan
- MUSIC Link Report
- Flood Information Certificate

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BRISBANE WATER LEGACY VILLAGE RESIDENTIAL APARTMENTS

51-57 MASONS PDE, POINT FREDERICK
INTERNAL CIVIL WORKS



LOCALITY PLAN

APPROXIMATE
LOCATION OF SITE





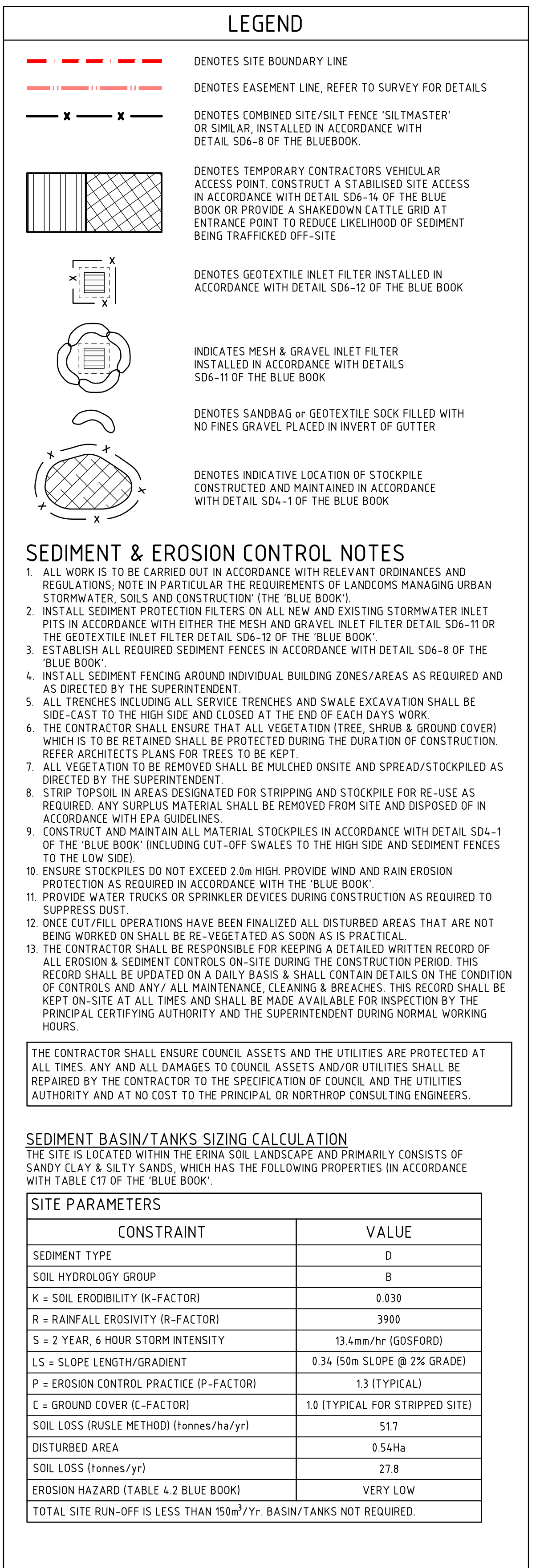
DRAWING SCHEDULE

DWG No.	DRAWING TITLE
C1.1	COVER SHEET
C2.1	CONCEPT SEDIMENT & EROSION CONTROL PLAN
C2.2	SEDIMENT & EROSION CONTROL DETAILS
C4.1	STORMWATER MANAGEMENT & LEVELS PLAN
C5.1	LONG SECTIONS & CROSS SECTIONS - SHEET 1
C6.1	VEHICLE SWEEP PATHS


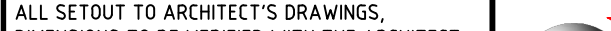
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DRAWN: KATHLEEN TURTON
DESIGNED: ROBERT SUCKLING
JOB MANAGER: DANIEL HOLLAND
VERIFIER:

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- SEDIMENT FENCE (SD 6-8)



CONSTRUCTION NOTES

- MESH AND GRAVEL INLET FILTER (SD 6-11)



CONSTRUCTION NOTES


- GEOTEXTILE INLET FILTER (SD 6-12)

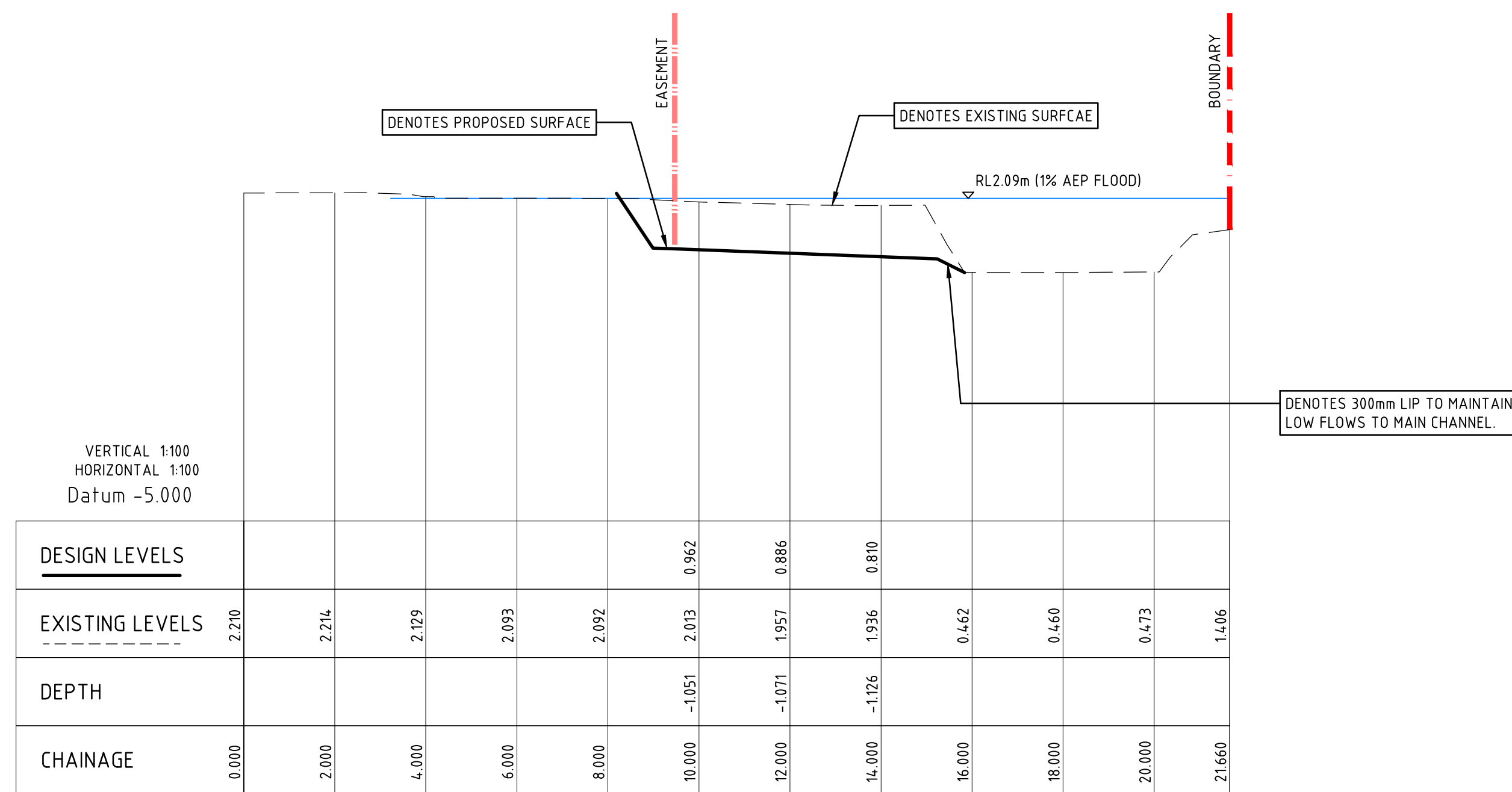


- STABILISED SITE ACCESS (SD 6-14)






- STOCKPILES (SD 4-1)

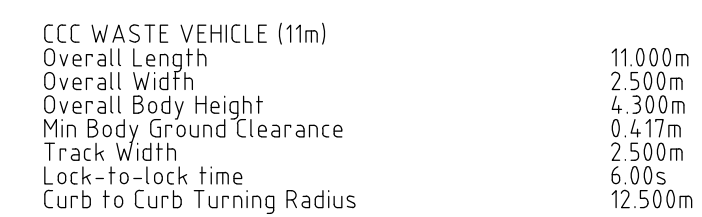
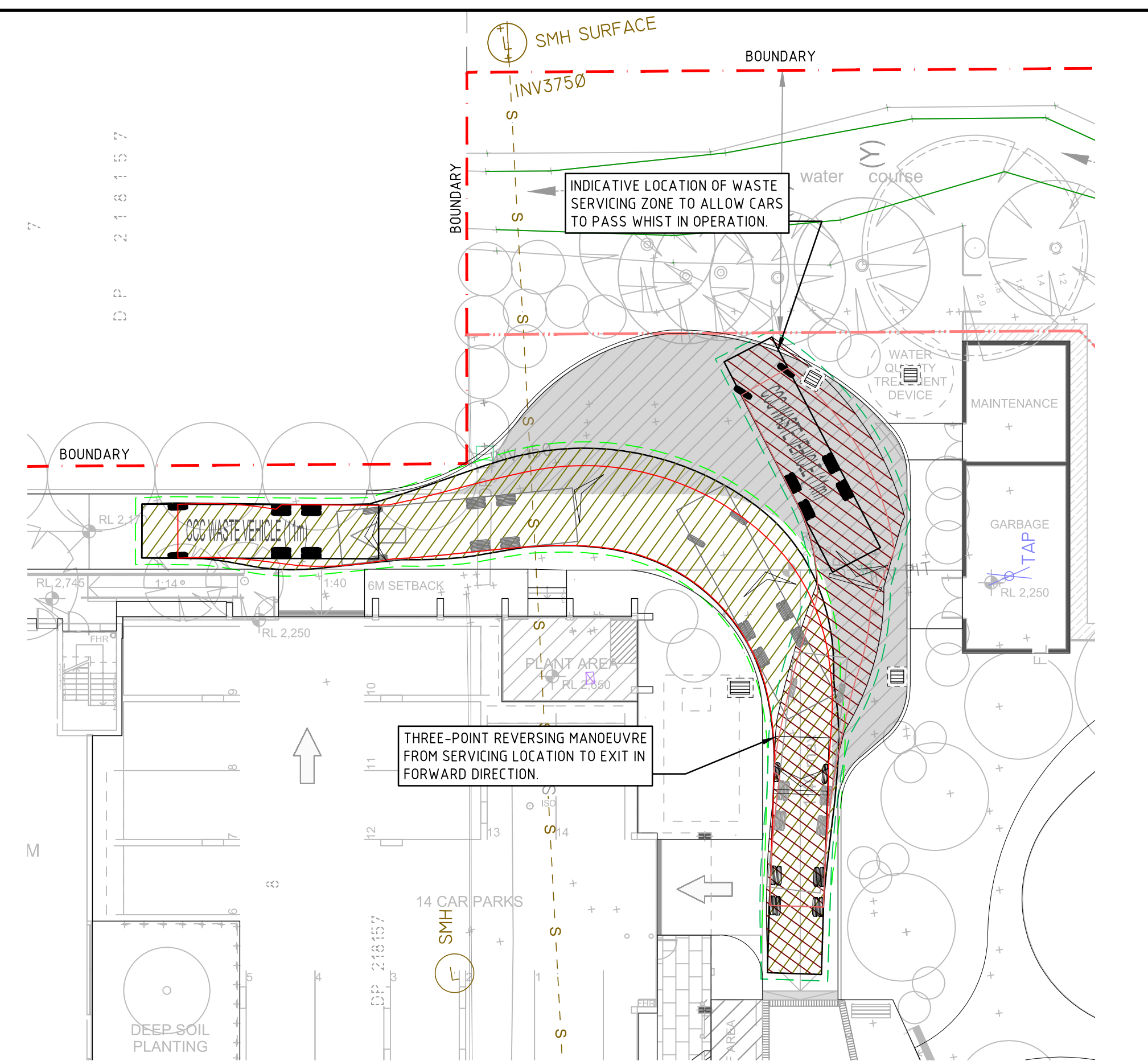
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The diagram shows a vehicle's footprint and its swept path. A solid black line represents the vehicle body extent. A dashed green line represents the wheel swept path. A red line indicates the 300mm clearance offset. A callout box points to the red line, stating "DENOTES 300mm CLEARANCE OFFSET". Another callout box points to the dashed green line, stating "DENOTES WHEEL SWEEP PATH". A third callout box points to the solid black line, stating "DENOTES VEHICLE BODY EXTENT". A fourth callout box points to the area between the solid black line and the dashed green line, stating "DENOTES WHEEL SWEEP PATH".

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PROJECT

**BRISBANE WATER LEGACY VILLAGE
RESIDENTIAL APPRATMENTS
51-57 MASONS PDE, POINT FREDERICK**

JOB NUMBER	
NL201088	
DRAWING NUMBER	REVISION
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MUSIC-*link* Report

Project Details		Company Details	
Project:	NL201088 51-57 Masons Parade	Company:	Northrop Consulting Engineers
Report Export Date:	10/09/2021	Contact:	Robert Suckling
Catchment Name:	NL201088 DA Issue_RS	Address:	Suite 4, 257-259 Central Coast Highway, Erina
Catchment Area:	0.608ha	Phone:	02 4365 1668
Impervious Area*:	61.91%	Email:	rsuckling@northrop.com.au
Rainfall Station:	66062 SYDNEY		
Modelling Time-step:	6 Minutes		
Modelling Period:	1/01/1974 - 31/12/1993 11:54:00 PM		
Mean Annual Rainfall:	1297mm		
Evapotranspiration:	1261mm		
MUSIC Version:	6.3.0		
MUSIC-link data Version:	6.33		
Study Area:	Lowland		
Scenario:	Central Coast Development		

* takes into account area from all source nodes that link to the chosen reporting node, excluding Import Data Nodes

Treatment Train Effectiveness		Treatment Nodes		Source Nodes	
Node: Post-Development Node	Reduction	Node Type	Number	Node Type	Number
Flow	30.5%	Rain Water Tank Node	1	Urban Source Node	6
TSS	80.7%	Sedimentation Basin Node	1		
TP	63.2%	Buffer Node	1		
TN	54.5%	GPT Node	1		
GP	91.1%	Generic Node	1		

Comments

Parameters reflective of precast chamber.

Passing Parameters

Node Type	Node Name	Parameter	Min	Max	Actual
Buffer	Buffer	Proportion of upstream impervious area treated	None	None	1
GPT	7 x OceanGuard200um	Hi-flow bypass rate (cum/sec)	None	99	0.14
Post	Post-Development Node	% Load Reduction	None	None	30.5
Post	Post-Development Node	GP % Load Reduction	90	None	91.1
Post	Post-Development Node	TN % Load Reduction	45	None	54.5
Post	Post-Development Node	TP % Load Reduction	45	None	63.2
Post	Post-Development Node	TSS % Load Reduction	80	None	80.7
Sedimentation	SF Manhole DN2250 (1.6m2)	Exfiltration Rate (mm/hr)	0	0	0
Sedimentation	SF Manhole DN2250 (1.6m2)	Extended detention depth (m)	0.25	1	0.77
Sedimentation	SF Manhole DN2250 (1.6m2)	High Flow Bypass Out (ML/yr)	None	None	0
Urban	Building Podium 0.017ha. 50% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Building Podium 0.017ha. 50% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Building Podium 0.017ha. 50% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Building Podium 0.017ha. 50% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Building Podium 0.017ha. 50% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.6	-0.6	-0.6
Urban	Building Podium 0.017ha. 50% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.15	2.15	2.15
Urban	Carpark 0.153ha 100% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Carpark 0.153ha 100% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Carpark 0.153ha 100% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Carpark 0.153ha 100% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.34	0.34	0.34
Urban	Carpark 0.153ha 100% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.3	-0.3	-0.3
Urban	Carpark 0.153ha 100% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.43	2.43	2.43
Urban	Driveway By-Pass 0.024ha 100% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Driveway By-Pass 0.024ha 100% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Driveway By-Pass 0.024ha 100% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Driveway By-Pass 0.024ha 100% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.34	0.34	0.34
Urban	Driveway By-Pass 0.024ha 100% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.3	-0.3	-0.3
Urban	Driveway By-Pass 0.024ha 100% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.43	2.43	2.43
Urban	Landscape 0.042ha. 0% Imp	Baseflow Total Nitrogen Mean (log mg/L)	-0.05	-0.05	-0.05
Urban	Landscape 0.042ha. 0% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-1.22	-1.22	-1.22
Urban	Landscape 0.042ha. 0% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.15	1.15	1.15
Urban	Landscape 0.042ha. 0% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Landscape 0.042ha. 0% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.66	-0.66	-0.66
Urban	Landscape 0.042ha. 0% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	1.95	1.95	1.95
Urban	Landscape 0.227 ha. 20% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.11	0.11	0.11
Urban	Landscape 0.227 ha. 20% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.85	-0.85	-0.85
Urban	Landscape 0.227 ha. 20% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.2	1.2	1.2
Urban	Landscape 0.227 ha. 20% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Landscape 0.227 ha. 20% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.6	-0.6	-0.6
Urban	Landscape 0.227 ha. 20% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	2.15	2.15	2.15

Only certain parameters are reported when they pass validation

NOTE: A successful self-validation check of your model does not constitute an approved model by Central Coast Council
MUSIC-*link* now in MUSIC by eWater – leading software for modelling stormwater solutions

Node Type	Node Name	Parameter	Min	Max	Actual
Urban	Roof 0.145ha. 100% Imp	Baseflow Total Nitrogen Mean (log mg/L)	0.32	0.32	0.32
Urban	Roof 0.145ha. 100% Imp	Baseflow Total Phosphorus Mean (log mg/L)	-0.82	-0.82	-0.82
Urban	Roof 0.145ha. 100% Imp	Baseflow Total Suspended Solids Mean (log mg/L)	1.1	1.1	1.1
Urban	Roof 0.145ha. 100% Imp	Stormflow Total Nitrogen Mean (log mg/L)	0.3	0.3	0.3
Urban	Roof 0.145ha. 100% Imp	Stormflow Total Phosphorus Mean (log mg/L)	-0.89	-0.89	-0.89
Urban	Roof 0.145ha. 100% Imp	Stormflow Total Suspended Solids Mean (log mg/L)	1.3	1.3	1.3
Only certain parameters are reported when they pass validation					

Failing Parameters

Node Type	Node Name	Parameter	Min	Max	Actual
Sedimentation	SF Manhole DN2250 (1.6m2)	Notional Detention Time (hrs)	8	12	0.0622
Sedimentation	SF Manhole DN2250 (1.6m2)	Total Nitrogen - k (m/yr)	500	500	1
Sedimentation	SF Manhole DN2250 (1.6m2)	Total Phosphorus - k (m/yr)	6000	6000	1
Sedimentation	SF Manhole DN2250 (1.6m2)	Total Suspended Solids - k (m/yr)	8000	8000	1

Only certain parameters are reported when they pass validation

Flood Information



26 March 2021

Dear Applicant,

I refer to your recent application for flood information. The information provided below is based on the available Council data at the time of application.

Property Details

Lot	51	DP	732632
Address	51-57 Masons Pde, Point Frederick NSW 2250		

Calculated Flood Levels

Flood event	Flood Level
PMF	3.52m AHD
1% AEP flood (1 in 100 Year Event)	2.37m AHD
5% AEP flood (1 in 20 Year Event)	2.10m AHD

Refer to glossary for definitions

The above flood levels represent the maximum flood level within the lot boundary. The flood data maps are attached in the appendix.

Source of Flooding information: Gosford CBD Local Overland Flood Study 2013, Brisbane Water Foreshore Flood Risk Management Study 2015

Minimum Floor Level (MFL)

The residential minimum floor level is **2.87m AHD**. The minimum floor level at this property is derived from the maximum 1% AEP Flood Level plus allowance for sea level rise plus 500mm freeboard. The minimum floor level may vary at different locations within the lot boundary.

State Environmental Planning Policy- SEPP (Exempt and Complying Development Codes) 2008

In accordance with State Environmental Planning Policy (Exempt and Complying Development Codes) 2008, if whole or part of the property is located within at least one of the exclusionary categories in Clause 3.5, development may not be permitted.

The table below contains hazard and hydraulic categorisation of the property in accordance with the NSW Floodplain Development Manual April 2005; Exclusionary categories listed in SEPP 2008, Clause 3.5

Hazard, Hydraulic, and SEPP 2008 exclusionary Categorisation



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Flood Information: 51-57 Masons Pde Pt Frederick

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Flood Information



1% AEP flood hazard	<input type="checkbox"/> H1 <input checked="" type="checkbox"/> H2 <input checked="" type="checkbox"/> H3 (Complying Development may not be permitted) <input type="checkbox"/> H4 (Complying Development may not be permitted) <input type="checkbox"/> H5 (Complying Development may not be permitted) <input type="checkbox"/> H6 (Complying Development may not be permitted) <input type="checkbox"/> N/A
Hydraulic categorisation	<input checked="" type="checkbox"/> All or part of the property is located in a floodway (Complying Development may not be permitted) <input checked="" type="checkbox"/> All or part of the property is located in a flood storage area (Complying Development may not be permitted) <input checked="" type="checkbox"/> All or part of property is located in a flood fringe <input type="checkbox"/> N/A
Exclusionary categories	<input checked="" type="checkbox"/> Flood Storage Area <input checked="" type="checkbox"/> Floodway Area <input type="checkbox"/> Flow path <input checked="" type="checkbox"/> High Hazard Area <input type="checkbox"/> High Risk Area <input type="checkbox"/> N/A (Complying Development may be permitted)

Disclaimer

Flood levels and minimum floor levels are provided in relation to Council's current records at the time of application. Council reserves the right to review and amend these levels from time to time. These amendments may impact the accuracy of information provided.



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Flood Information: 51-57 Masons Pde Pt Frederick

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Glossary

AHD	Australian Height Datum is a common national surface level datum approximately corresponding to mean sea level.
PMF	The Probable Maximum Flood is the largest flood that could conceivably occur.
1% AEP flood	The 1% Annual Exceedance Probability flood has a 1% (1:100) probability of occurring in any given year. This flood is also known as 1 in 100, 100yr ARI or Q100.
2% AEP flood	The 2% Annual Exceedance Probability flood has a 2% (1:50) probability of occurring in any given year. This flood is also known as 1 in 50, 50yr ARI or Q50.
5% AEP flood	The 5% Annual Exceedance Probability flood has a 5% (1:20) probability of occurring in any given year. This flood is also known as 1 in 20, 20yr ARI or Q20.
H1 Hazard Categorisation*	Generally safe for people, vehicles and buildings
H2 Hazard Categorisation*	Unsafe for small vehicles
H3 Hazard Categorisation*	Unsafe for vehicles, children and the elderly
H4 Hazard Categorisation*	Unsafe for people and vehicles
H5 Hazard Categorisation*	Unsafe for vehicles and people. All buildings vulnerable to structural damage. Some less robust building types vulnerable to failure
H6 Hazard Categorisation*	Unsafe for vehicles and people. All building types considered vulnerable to failure
Floodways*	Those areas where a significant volume of water flows during floods and are often aligned with obvious natural channels. They are areas that, even if only partially blocked, would cause a significant increase in flood levels and/or a significant redistribution of flood flow, which may in turn adversely affect other areas. They are often, but not necessarily, areas with deeper flow or areas where higher velocities occur.
Flood storage*	Those parts of the floodplain that are important for the temporary storage of floodwaters during the passage of flood. If the capacity of a flood storage area is substantially reduced by, for example, the construction of levees or by landfill, flood levels in nearby areas may rise and the peak discharge downstream may be increased. Substantial reduction of the capacity of a flood storage area can also cause a significant redistribution of flood flows.
Flood fringe*	The remaining area of land affected by flooding, after floodway and flood storage areas have been defined.

Source – NSW Floodplain Development Manual April 2005

Hydraulic Hazard AIDR ref <https://knowledge.aidr.org.au/media/3518/adr-guideline-7-3.pdf>

NSW FDM ref <https://www.environment.nsw.gov.au/topics/water/floodplains/floodplain-manual>



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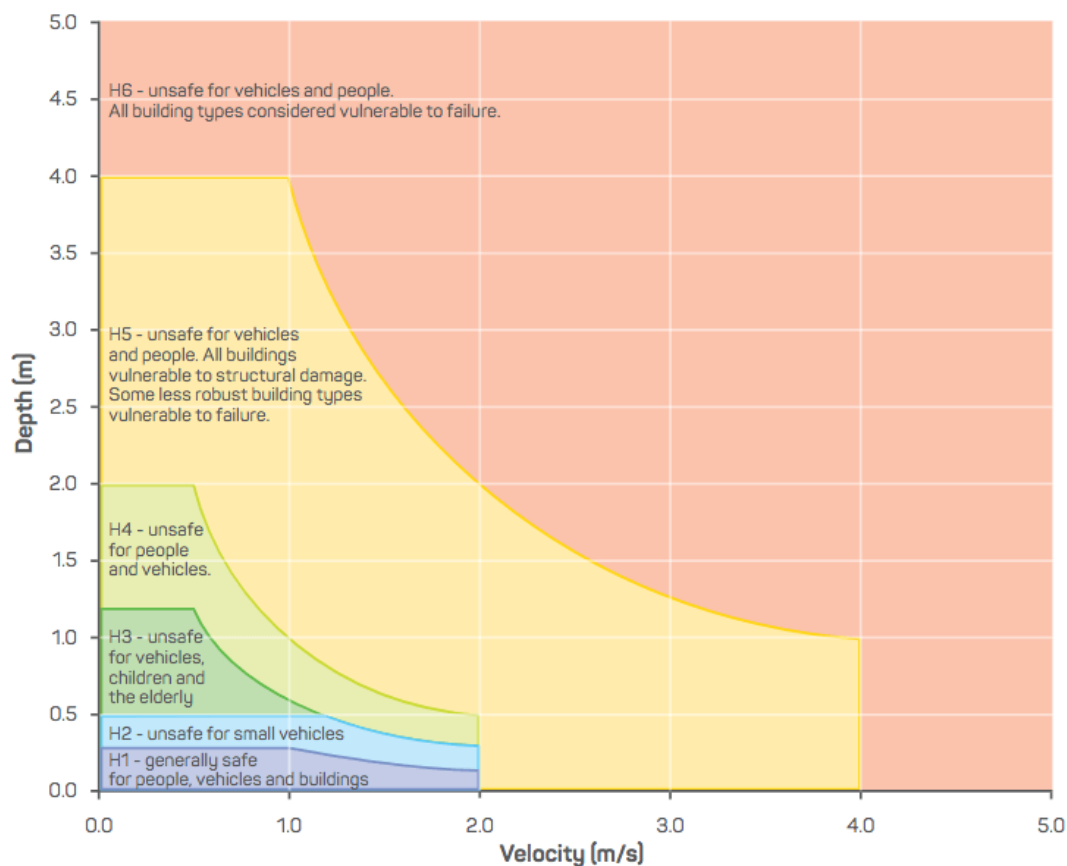
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Flood Information: 51-57 Masons Pde Pt Frederick

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Flood Information



Source – Australian Institute for Disaster Resilience 2017. Hydraulic Hazard: refer also to Australian Rainfall and Runoff Section 7.2.7 General Flood Hazard Curves (Figure 6.7.9) <http://book.arr.org.au.s3-website-ap-southeast-2.amazonaws.com/>

The information provided in this letter is provided only to you and is not intended to be provided to a third party.

Should you have any enquiries concerning this letter, please do not hesitate to contact Andrew Dewar on 1300 463 954 during the hours of 8.30am to 5.00pm Monday to Friday.

Yours faithfully,

Andrew Dewar
Floodplain Development Engineer

Phone: 1300 463 954



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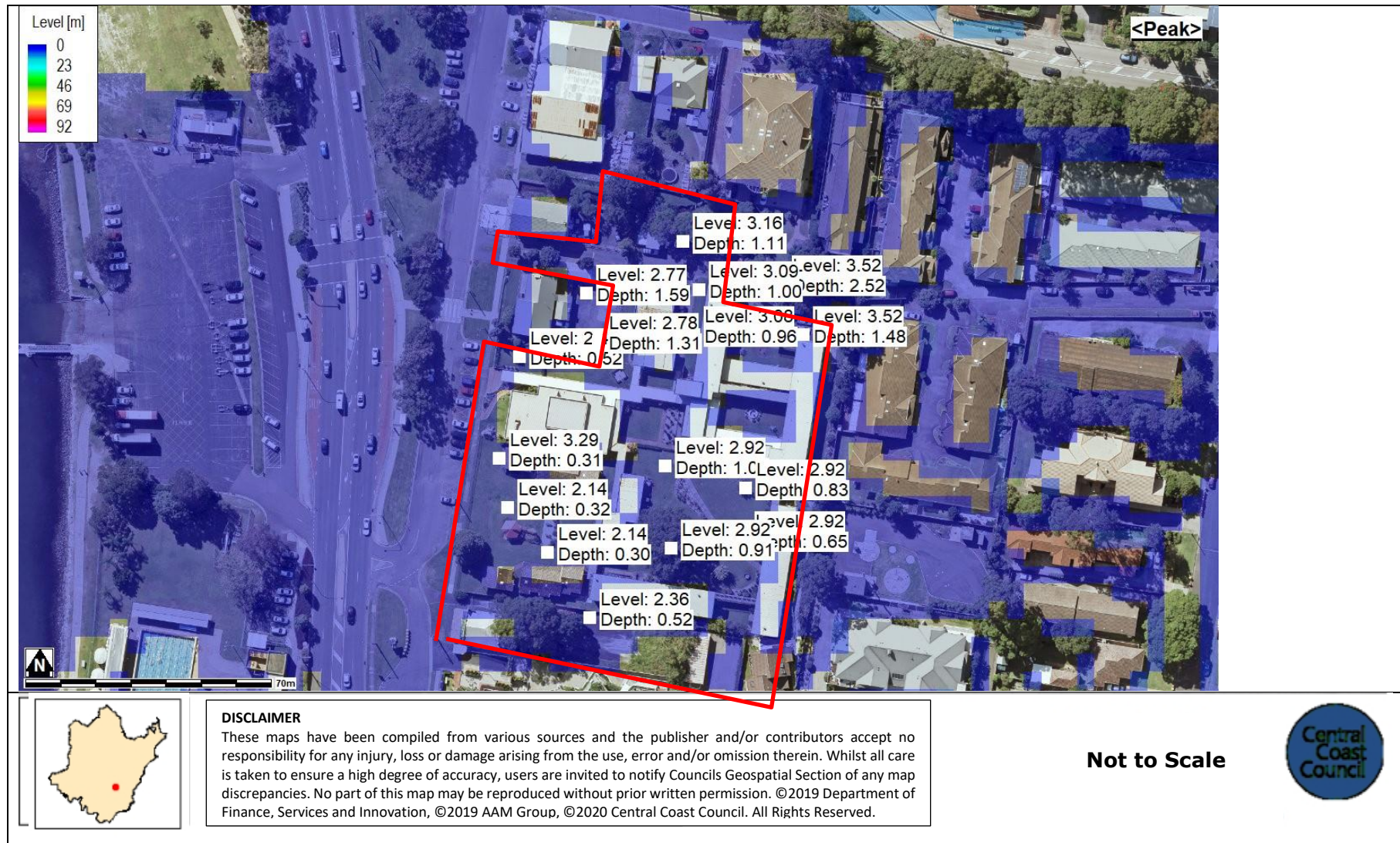
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Appendix

PMF Flood Extent



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Gosford Office: 49 Mann St / PO Box 21 Gosford NSW 2250

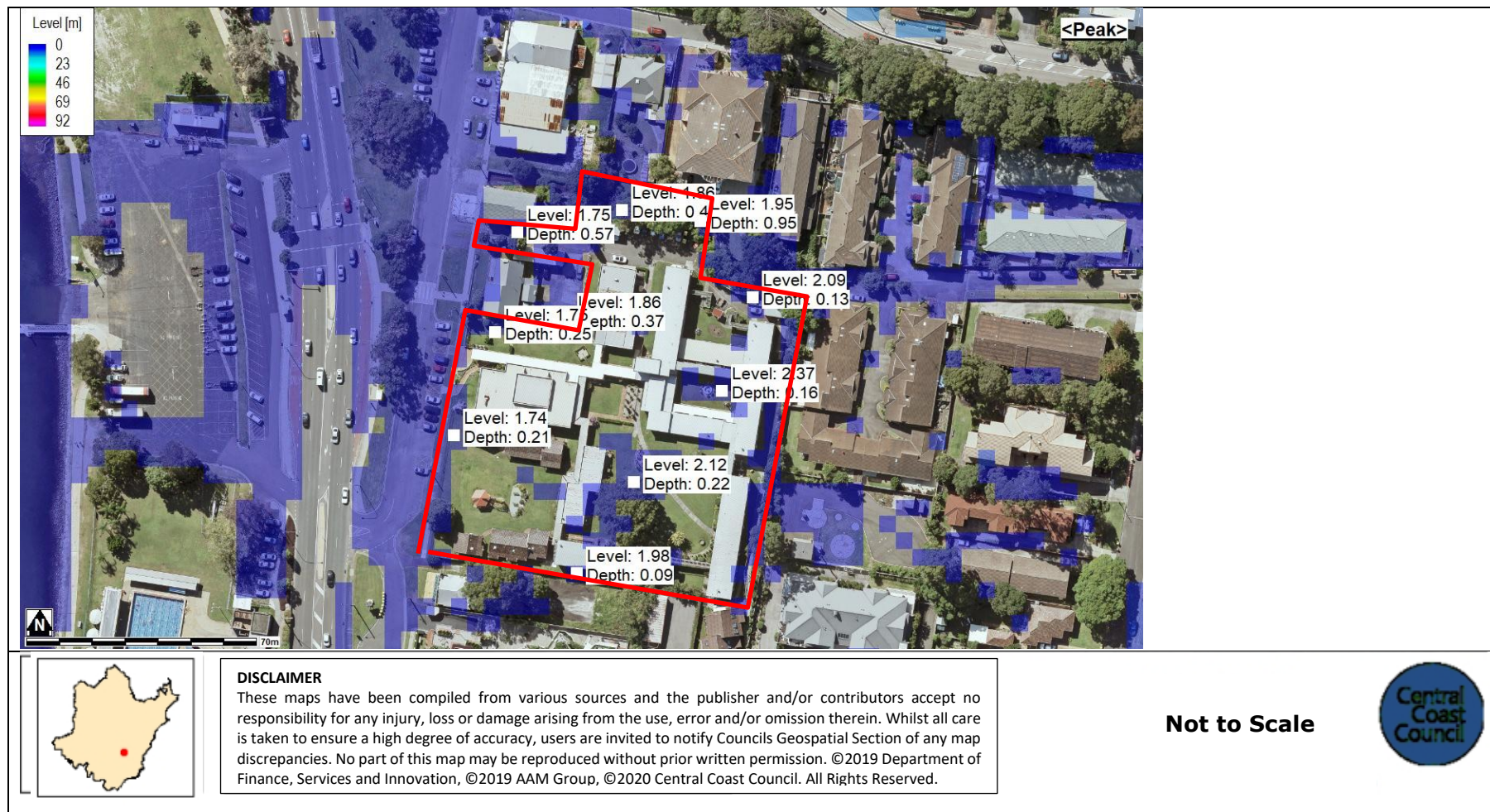
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Flood Information

1% AEP Flood Extent



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Flood Information: 51-57 Masons Pde Pt Frederick

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Flood Information

5% AEP Flood Extents



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Flood Information: 51-57 Masons Pde Pt Frederick

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Flood Information

Hazard Categorisation



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Not to Scale



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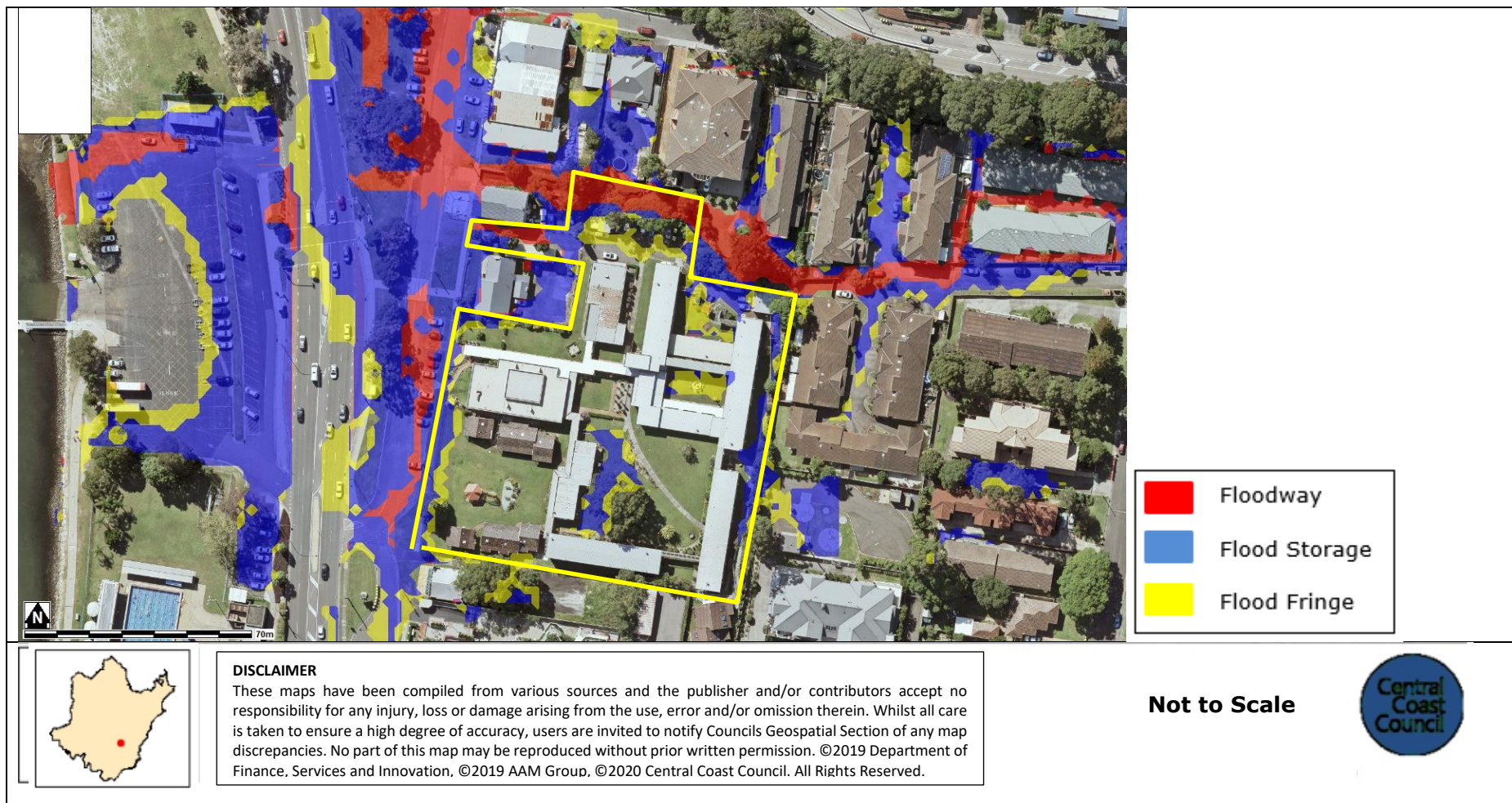
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Flood Information

Hydraulic Categorisation



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BRISBANE WATER LEGACY VILLAGE RESIDENTIAL APARTMENTS

51-57 MASONS PDE, POINT FREDERICK
INTERNAL CIVIL WORKS



LOCALITY PLAN

APPROXIMATE
LOCATION OF SITE





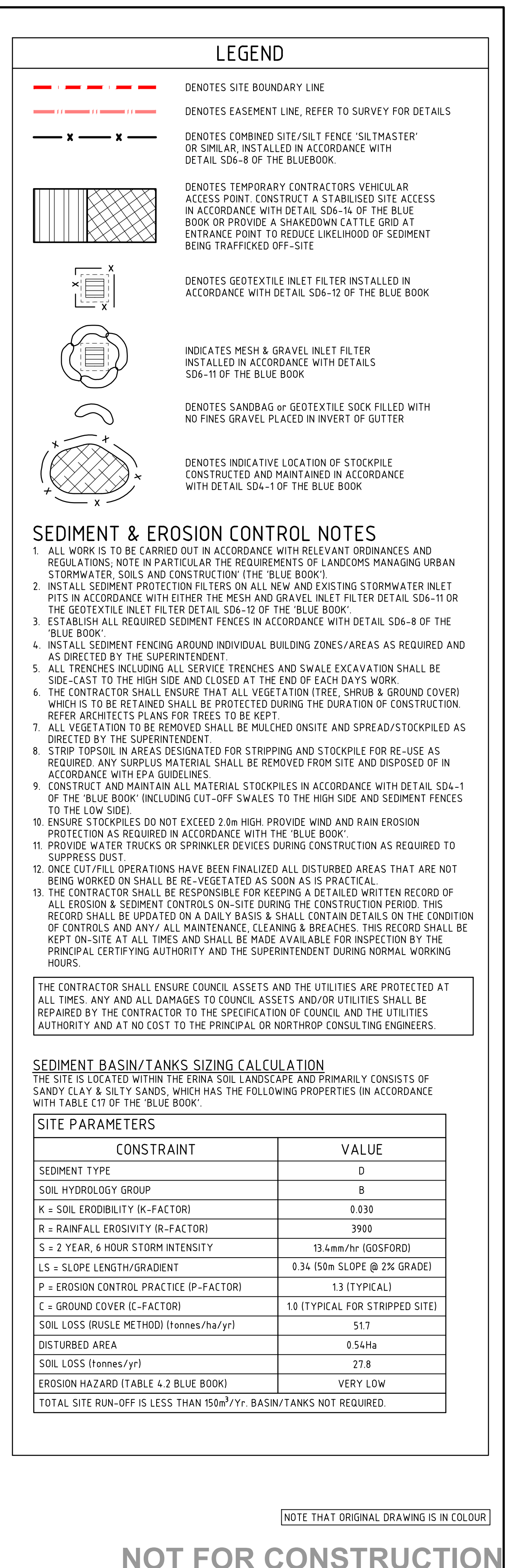
DRAWING SCHEDULE



DWG No.	DRAWING TITLE
C1.1	COVER SHEET
C2.1	CONCEPT SEDIMENT & EROSION CONTROL PLAN
C2.2	SEDIMENT & EROSION CONTROL DETAILS
C4.1	STORMWATER MANAGEMENT & LEVELS PLAN
C5.1	LONG SECTIONS & CROSS SECTIONS - SHEET 1
C6.1	VEHICLE SWEEP PATHS

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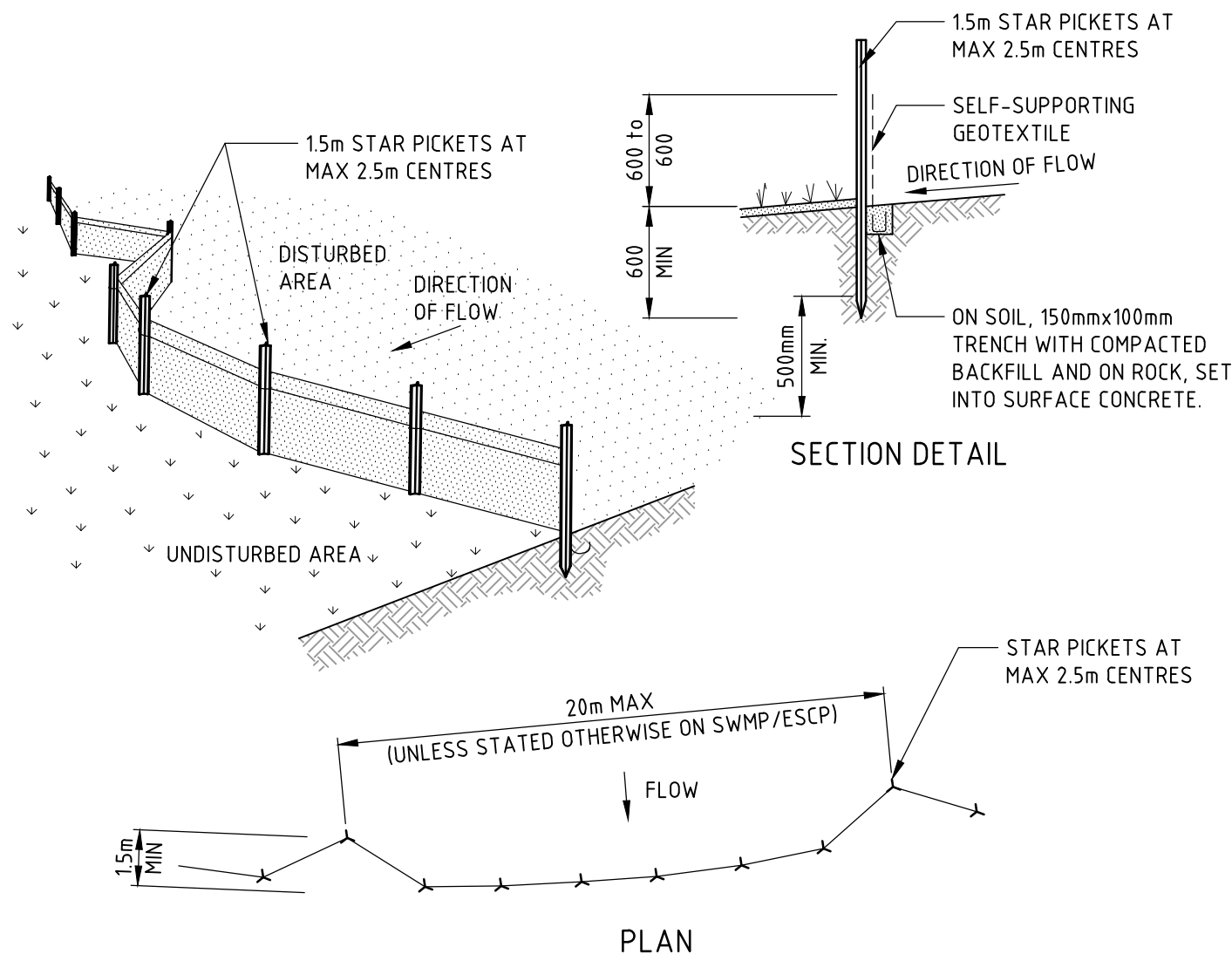
DRAWN: KATHLEEN TURTON
DESIGNED: ROBERT SUCKLING
JOB MANAGER: DANIEL HOLLAND
VERIFIER:

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE	CLIENT	ARCHITECT		PROJECT	DRAWING TITLE	JOB NUMBER				
A	DEVELOPMENT APPLICATION	KT		DH	21.05.21		INTEGRATED DESIGN GROUP	<div>ALL SETOUT TO ARCHITECT'S DRAWINGS. DIMENSIONS TO BE VERIFIED WITH THE ARCHITECT AND ON SITE BEFORE MAKING SHOP DRAWINGS OR COMMENCING WORK. NORTHROP ACCEPTS NO RESPONSIBILITY FOR THE USABILITY, COMPLETENESS OR SCALE OF DRAWINGS TRANSFERRED ELECTRONICALLY.</div>	 <div>Central Coast Suite 4, 257-259 Central Coast Hwy, Erina NSW 2250 Ph (02) 4365 1668 Fax (02) 4367 6555 Email centralcoast@northrop.com.au ABN 81 094 433 100</div>	BRISBANE WATER LEGACY VILLAGE RESIDENTIAL APPRATMENTS 51-57 MASONS PDE, POINT FREDERICK	INTERNAL CIVIL WORKS COVER SHEET	NL201088			
B	DEVELOPMENT APPLICATION	KT		DH	15.09.21								DRAWING NUMBER	REVISION	
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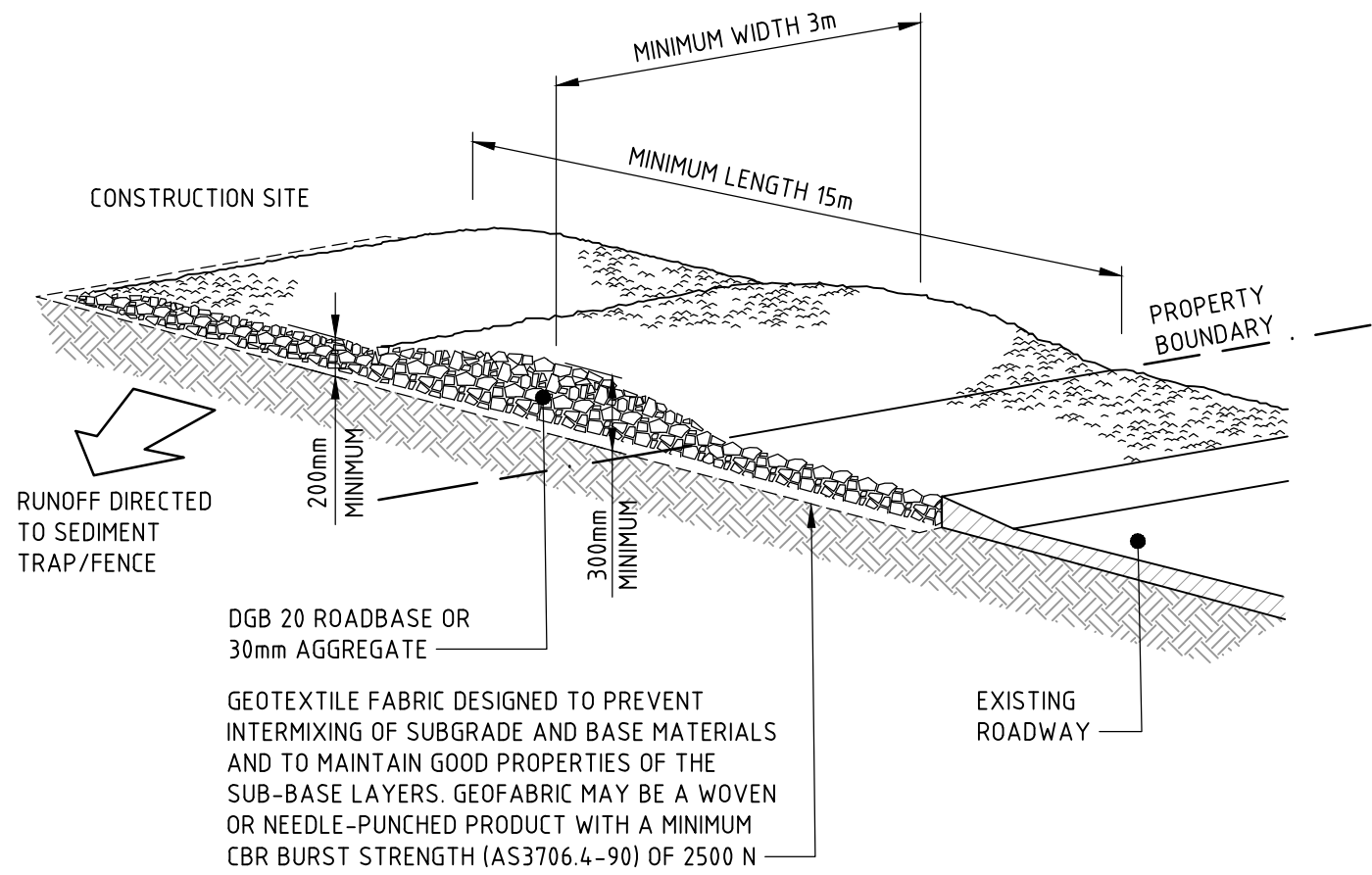
DRAWN: KATHLEEN TURTON DESIGNED: ROBERT SUCKLING JOB MANAGER: DANIEL HOLLAND VERIFIER:



CONSTRUCTION NOTES

1. CONSTRUCT SEDIMENT FENCES AS CLOSE AS POSSIBLE TO BEING PARALLEL TO THE CONTOURS OF THE SITE, BUT WITH SMALL RETURNS AS SHOWN IN THE DRAWING TO LIMIT THE CATCHMENT AREA OF ANY ONE SECTION. THE CATCHMENT AREA SHOULD BE SMALL ENOUGH TO LIMIT WATER FLOW IF CONCENTRATED AT ONE POINT TO 50 LITRES PER SECOND IN THE DESIGN STORM EVENT, USUALLY THE 10-YEAR EVENT.
2. CUT A 150mm DEEP TRENCH ALONG THE UPSLOPE LINE OF THE FENCE FOR THE BOTTOM OF THE FABRIC TO BE ENTRENCHED.
3. DRIVE 15 METRE LONG STAR PICKETS INTO GROUND AT 2.5 METRE INTERVALS (MAX) AT THE DOWNSLOPE EDGE OF THE TRENCH. ENSURE ANY STAR PICKETS ARE FITTED WITH SAFETY CAPS.
4. FIX SELF-SUPPORTING GEOTEXTILE TO THE UPSLOPE SIDE OF THE POSTS ENSURING IT GOES TO THE BASE OF THE TRENCH. FIX THE GEOTEXTILE WITH WIRE TIES OR AS RECOMMENDED BY THE MANUFACTURER. ONLY USE GEOTEXTILE SPECIFICALLY PRODUCED FOR SEDIMENT FENCING. THE USE OF SHADE CLOTH FOR THIS PURPOSE IS NOT SATISFACTORY.
5. JOIN SECTIONS OF FABRIC AT A SUPPORT POST WITH A 150mm OVERLAP.
6. BACKFILL THE TRENCH OVER THE BASE OF THE FABRIC AND COMPACT IT THOROUGHLY OVER THE GEOTEXTILE.

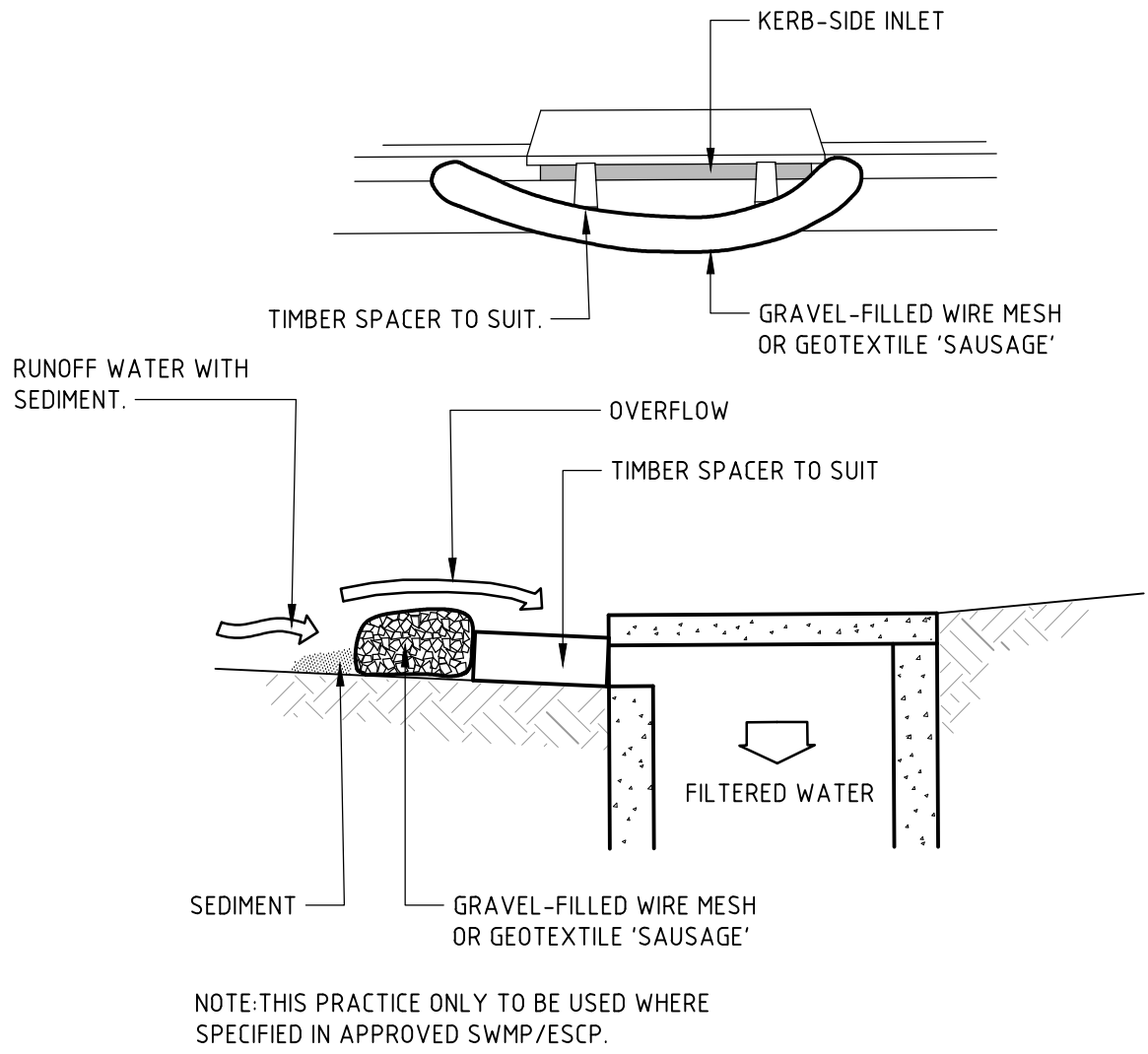
SEDIMENT FENCE (SD 6-8)



CONSTRUCTION NOTES

1. STRIP THE TOPSOIL, LEVEL THE SITE AND COMPACT THE SUBGRADE.
2. COVER THE AREA WITH NEEDLE-PUNCHED GEOTEXTILE.
3. CONSTRUCT A 200mm THICK PAD OVER THE GEOTEXTILE USING ROAD BASE OR 30mm AGGREGATE.
4. ENSURE THE STRUCTURE IS AT LEAST 15 METRES LONG OR TO BUILDING ALIGNMENT AND AT LEAST 3 METRES WIDE.
5. WHERE A SEDIMENT FENCE JOINS ONTO THE STABILISED ACCESS, CONSTRUCT A HUMP IN THE STABILISED ACCESS TO DIVERT WATER TO THE SEDIMENT FENCE.

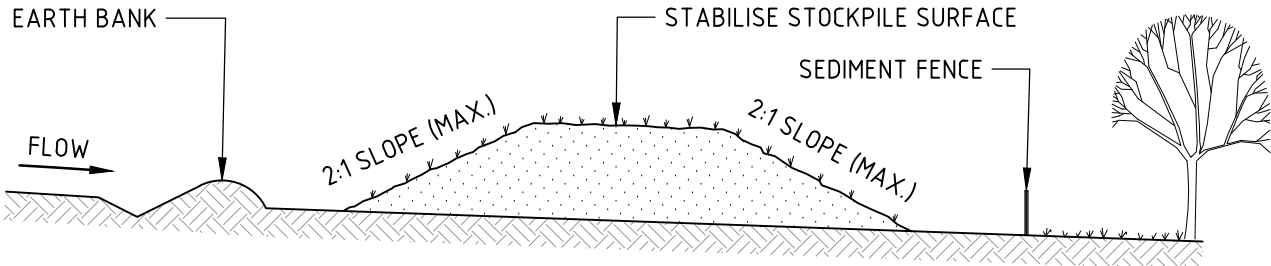
STABILISED SITE ACCESS (SD 6-14)



CONSTRUCTION NOTES

1. INSTALL FILTERS TO KERB INLETS ONLY AT SAG POINTS.
2. FABRICATE A SLEEVE MADE FROM GEOTEXTILE OR WIRE MESH LONGER THAN THE LENGTH OF THE INLET PIT AND FILL IT WITH 25mm TO 50mm GRAVEL.
3. FORM AN ELLIPTICAL CROSS-SECTION ABOUT 150mm HIGH x 400mm WIDE.
4. PLACE THE FILTER AT THE OPENING LEAVING AT LEAST A 100mm SPACE BETWEEN IT AND THE KERB INLET. MAINTAIN THE OPENING WITH SPACER BLOCKS.
5. FORM A SEAL WITH THE KERB TO PREVENT SEDIMENT BYPASSING THE FILTER.
6. SANDBAGS FILLED WITH GRAVEL CAN SUBSTITUTE FOR THE MESH OR GEOTEXTILE PROVIDING THEY ARE PLACED SO THAT THEY FIRMLY ABUT EACH OTHER AND SEDIMENT-LADEN WATERS CANNOT PASS BETWEEN.

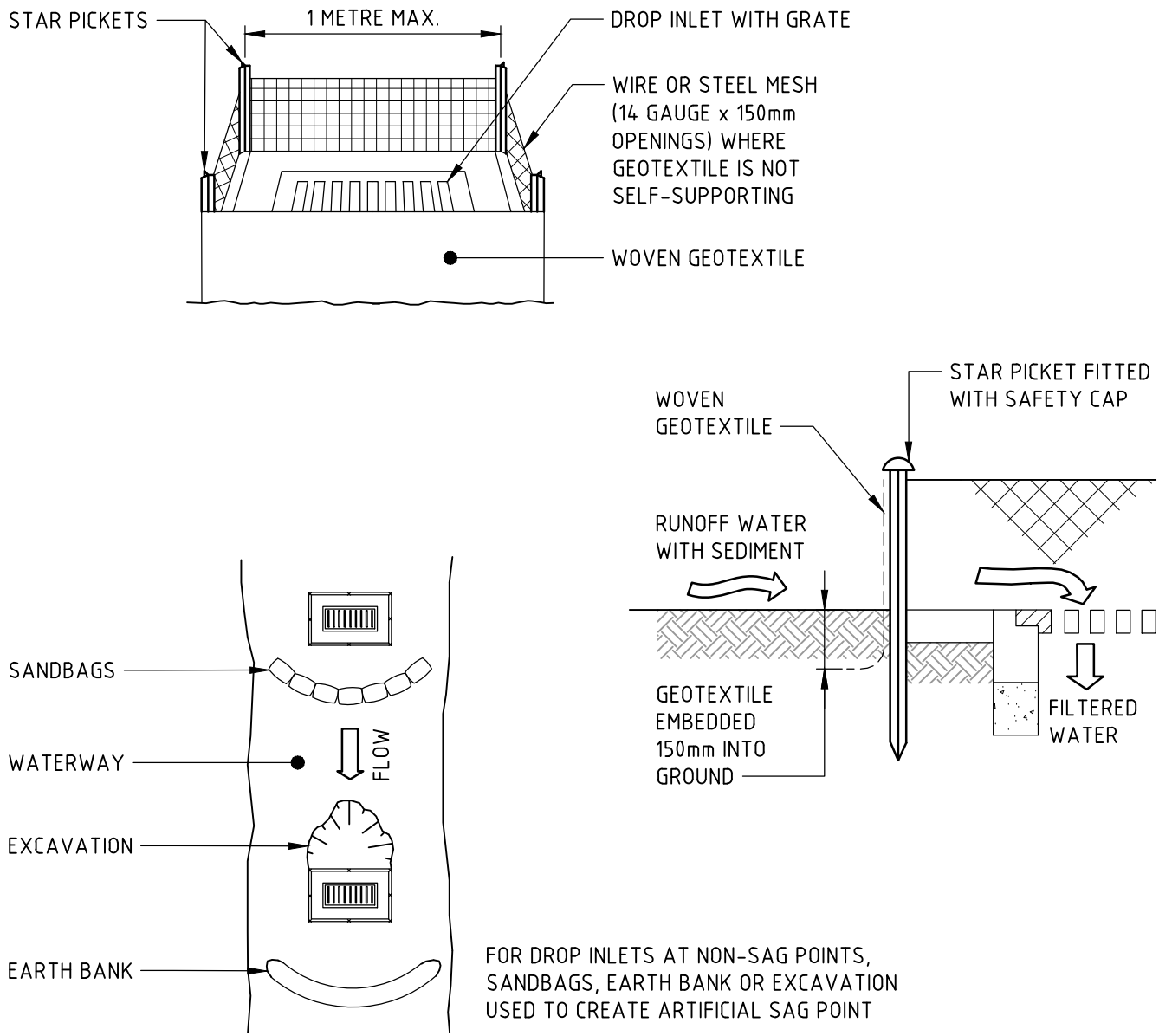
MESH AND GRAVEL INLET FILTER (SD 6-11)



CONSTRUCTION NOTES

1. PLACE STOCKPILES MORE THAN 2m (PREFERABLY 5m) FROM EXISTING VEGETATION, CONCENTRATED WATER FLOW, ROADS AND HAZARD AREAS.
2. CONSTRUCT ON THE CONTOUR AS LOW, FLAT, ELONGATED MOUNDS.
3. WHERE THERE IS SUFFICIENT AREA, TOPSOIL STOCKPILES SHALL BE LESS THAN 2m IN HEIGHT.
4. WHERE THEY ARE TO BE IN PLACE FOR MORE THAN 10 DAYS, STABILISE FOLLOWING THE APPROVED ESCP OR SWMP TO REDUCE THE C-FACTOR TO LESS THAN 0.10.
5. CONSTRUCT EARTH BANKS (STANDARD DRAWING 5-5) ON THE UPSLOPE SIDE TO DIVERT WATER AROUND STOCKPILES AND SEDIMENT FENCES (STANDARD DRAWING 6-8) 1 TO 2m DOWNSLOPE.

STOCKPILES (SD 4-1)





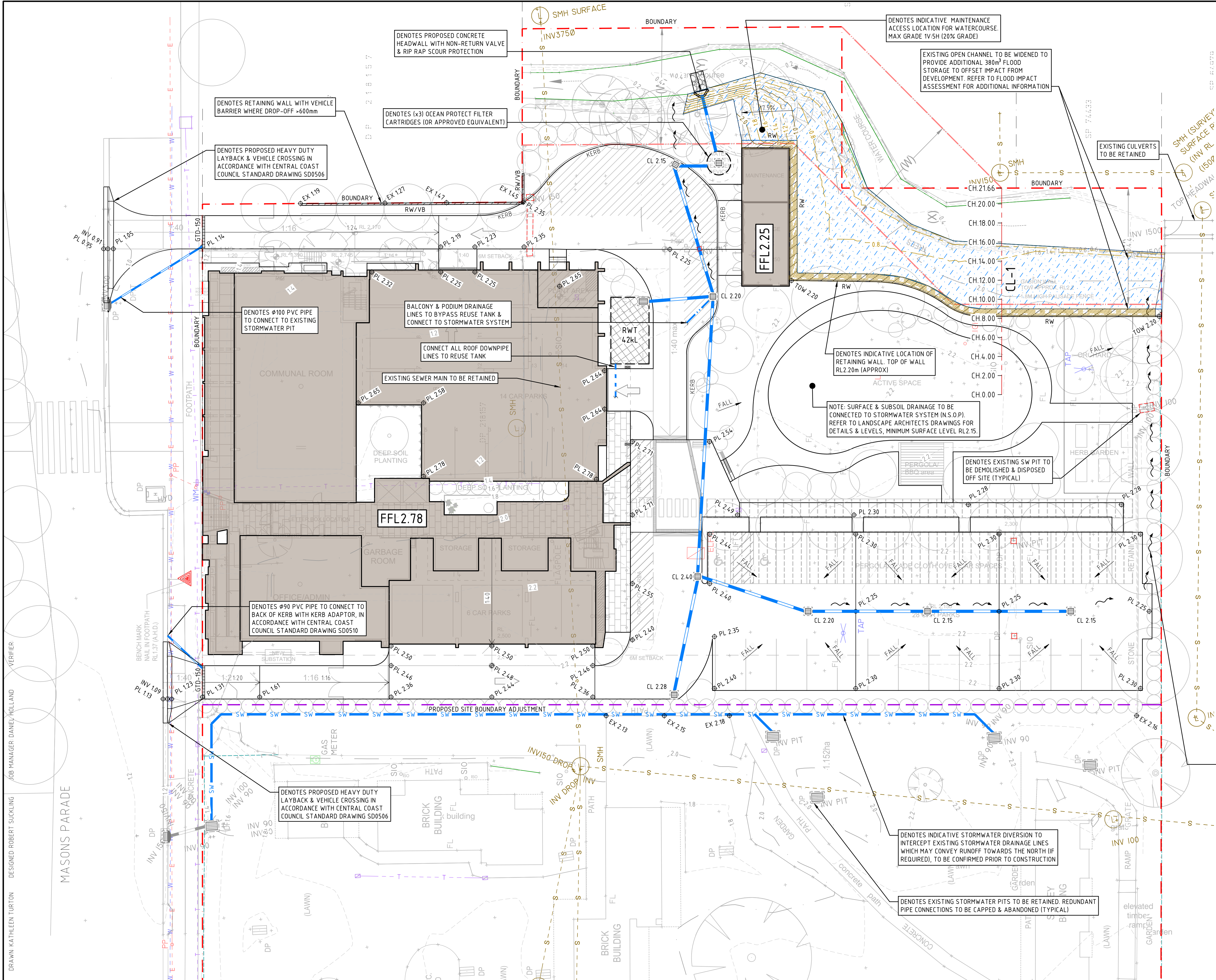
CONSTRUCTION NOTES

1. FABRICATE A SEDIMENT BARRIER MADE FROM GEOTEXTILE OR STRAW BALES.
2. FOLLOW STANDARD DRAWING 6-7 AND STANDARD DRAWING 6-8 FOR INSTALLATION PROCEDURES FOR THE STRAW BALES OR GEOFABRIC. REDUCE THE PICKET SPACING TO 1 METRE CENTRES.
3. IN WATERWAYS, ARTIFICIAL SAG POINTS CAN BE CREATED WITH SANDBAGS OR EARTH BANKS AS SHOWN IN THE DRAWING.
4. DO NOT COVER THE INLET WITH GEOTEXTILE UNLESS THE DESIGN IS ADEQUATE TO ALLOW FOR ALL WATERS TO BYPASS IT.

GEOTEXTILE INLET FILTER (SD 6-12)

NOT FOR CONSTRUCTION

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LEGEND

DENOTES SITE BOUNDARY LINE

DENOTES EASEMENT LINE, REFER TO SURVEY FOR DETAILS

DENOTES PROPOSED BUILDING EXTENTS, REFER TO ARCHITECTURAL & STRUCTURAL DRAWINGS FOR DETAILS

DENOTES PROPOSED FINISHED FLOOR LEVEL

DENOTES PROPOSED FINISHED SURFACE LEVEL

DENOTES PROPOSED STORMWATER PIT COVER LEVEL

DENOTES EXISTING SURFACE LEVEL

DENOTES EXISTING CONTOURS

DENOTES DESIGN CONTOURS

DENOTES ALIGNMENT CONTROL LINE & CHAINAGE, REFER TO LONG SECTION

DENOTES PROPOSED STORMWATER PIT. ALL NEW STORMWATER INLET PITS ARE TO BE FITTED WITH FILTER INSERTS IN ACCORDANCE WITH MANUFACTURERS SPECIFICATION

DENOTES EXISTING STORMWATER PIT / KERB INLET PIT TO BE RETAINED

DENOTES GRATED TRENCH DRAIN & WIDTH

DENOTES CONCRETE HEADWALL WITH NON-RETURN VALVE AND RIP RAP SCOUR PROTECTION

DENOTES BELOW GROUND RAINWATER TANK/S WITH 42KL COMBINED CAPACITY. HARVESTED RAINWATER TO BE USED FOR IRRIGATION & TOILET FLUSHING

DENOTES PROPOSED STORMWATER LINE

DENOTES OVERLAND FLOW PATH

DENOTES RETAINING WALL WITH VEHICLE BARRIER (REQUIRED FOR DROP-OFFS GREATER THEN 600mm)

DENOTES APPROXIMATE LOCATION OF EXISTING ELECTRICITY LINE

DENOTES APPROXIMATE LOCATION OF EXISTING GAS MAIN

DENOTES APPROXIMATE LOCATION OF EXISTING TELECOMMUNICATION LINE

DENOTES APPROXIMATE LOCATION OF EXISTING WATER MAIN

DENOTES APPROXIMATE LOCATION OF EXISTING SEWER MAIN

LOCATIONS OF EXISTING SERVICES ARE APPROXIMATE ONLY & MAY NOT BE COMPLETE. THE BUILDER IS RESPONSIBLE FOR LOCATING EXISTING INFRASTRUCTURE (CULVERTS, PITS, PIPES, SERVICES, INVERT & COVER LEVELS ETC) PRIOR TO COMMENCING CONSTRUCTION.

THE BUILDER SHALL ALLOW TO MODIFY ALL EXISTING SERVICE COVERS TO MATCH THE NEW PAVEMENTS, IN ACCORDANCE WITH THE RELEVANT AUTHORITIES REQUIREMENTS.

PROVIDE TEMPORARY TRAFFIC CONTROL IN ACCORDANCE WITH STATE & FEDERAL STATUTORY REQUIREMENTS AND LOCAL COUNCIL SPECIFICATIONS/REQUIREMENTS

NOTE: ALL LEVELS TO AUSTRALIAN HEIGHT DATUM (AHD). ORIGIN OF LEVELS PM 19217, RL1564

DRAWINGS TO BE READ IN CONJUNCTION WITH CONCEPT STORMWATER MANAGEMENT REPORT & FLOOD IMPACT ASSESSMENT

DENOTES INDICATIVE OVERLAND FLOW PATH TO BE FREE OF OBSTRUCTIONS

DRAWN: KATHLEEN TURTON
DESIGNED: ROBERT SUCKLING
JOB MANAGER: DANIEL HOLLAND
VERIFIER:

REVISION	DESCRIPTION	ISSUED	VER'D	APP'D	DATE
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ARCHITECT
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PLANS 1:200@A1

Central Coast
Suite 4, 257-259 Central Coast Hwy, Erina NSW 2250
Ph (02) 4365 1668 Fax (02) 4367 6555
Email centralcoast@northrop.com.au ABN 81 094 433 100

PROJECT
**BRISBANE WATER LEGACY VILLAGE
RESIDENTIAL APPRATMENTS
51-57 MASONS PDE, POINT FREDERICK**

DRAWING TITLE
**INTERNAL CIVIL WORKS
STORMWATER MANAGEMENT
& LEVELS PLAN**

JOB NUMBER
NL201088

DRAWING NUMBER
C4.1

REVISION
B

DRAWING SHEET SIZE = A1

NOTE THAT ORIGINAL DRAWING IS IN COLOUR



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